



Clean Air Engineering

FIELD HANDBOOK

1st EDITION

1/1/93

REVISION 1 - 8/9/95

REVISION 2 - 1/14/98

REVISION HISTORY

Revision 1 - 8/9/95

TOC - Equation for excess air correction added to Emission section and Relative Humidity added to the Moisture Section.

Page 6 - Equation B7 is now also written in terms of Dn.

Page 9 - Page reference corrected.

Page 11 - Equation E2 clarified. ppm measured must be on a dry basis.

Page 11 - Equation E4 - units for Fc corrected to scf/MBtu. Also, the equation was clarified - %CO₂ and concentration of pollutant must be on the same moisture basis - both wet or both dry.

Page 12 - Correction to a percent excess air added.

Page 16 - Equation F3 - Molecular weight of water changed from 18 to 18.01.

Page 17 - Note added for calculating the relative humidity based on wet bulb and dry bulb temperatures.

Page 17 - Equation F4 - Clarified by stating temperatures are in Fahrenheit.

Page 20 - Equation G3 corrected. The constant 0.75 was corrected to 0.075; and 0.01060 was corrected to 0.001060.

Page 28 - Comment on blank correction added.

Revisions 2 - 1/14/98

Page 19 - Critical orifice procedure modified.

PREFACE

This is the first edition of the *Field Handbook*. This manual is designed to provide practical help to those working in the field and for use in-house as a reference. Similar equations are grouped together with the variable names indexed on the following page.

Current plans for the next edition include adding calculations for:

- PM₁₀ (Method 201A)
- Anderson Impactor
- Cyclade for particle sizing
- 3D Calculations

Contact Dave Nasralla with any equations you feel would make a helpful contribution.

The following codes are used through out the manual for references:

SSPP Student Manual.....	EPA APTI Course 450 Source Sampling for Particulate Pollutants - EPA 450/2-79-006 by J.A. Janke and G.J. Aldina
PH.....	Perry's Chemical Engineer's Handbook, Sixth Edition, McGraw Hill, 1984.
EPA.....	Title 40 of the Code of Federal Regulations, Part 60, Appendix A. July 1st, 1992.
QAH.....	The Quality Assurance Handbook for Air Pollution Measurement Systems, Vol III, Stationary Source Specific Methods. EPA 600/9- 9-76-005.



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Method 5 K Factor

1

Information required:	Variable	Example	Units
From the meter card:	H@	1.817	
Expected meter temp:	T _m	71	°F
Stack temp:	T _s	459	°F
Static Pressure of Stack:	P _{static}	-0.20	" H ₂ O
Barometric Pressure:	P _b	29.62	" Hg
Oxygen:	%O ₂	9.2	%
Carbon Dioxide:	%CO ₂	11.7	%
Nitrogen:	%N ₂	79.1	%
Carbon Monoxide:	%CO	0.0	%
Moisture Content Estimate:	B _{wo}	0.053	none
Pitot tube calibration factor:	C _p	0.84	none
Root P average:	$\sqrt{P_{ave}}$	0.90	root "H ₂ O
The square of the root P average:	P	0.81	"H ₂ O
Diameter of available nozzle:	D _n	0.276	inches
Desired meter flow rate:	H	1.8	"H ₂ O
Meter correction factor:	Yd:	1.0050	

Preliminary Calculations

A1. Absolute pressure of stack gas:

EPA M2- Eq. 2-6 and PH

$$P_s = P_b + \frac{P_{static} \frac{"H_2O}{13.6}}{\frac{"H_2O}{13.6}} = 29.62 + \frac{-0.20}{13.6} = 29.605 \text{ inches Hg}$$

A2. Molecular weight of gas (dry):

EPA M3- Eq. 3-1

$$M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%CO + \%N)$$

$$= 0.44(11.7) + 0.32(9.2) + 0.28(0 + 79.1) = 30.24 \text{ lb/lb} \cdot \text{mole}$$

A3. Molecular weight of gas (wet):

EPA M2- Eq. 2-5

$$M_s = M_d (1 - B_{wo}) + 18 (B_{wo})$$

$$= 30.24 (1 - 0.053) + 18(0.053) = 29.59 \text{ lb/lb} \cdot \text{mole}$$

Method 5 K Factor (Continued)

Nozzle size, K factor and V_{mstd} determination

An example hand calculation can be found on the following page.

A4. Ideal nozzle size (squared) based on the V_{mstd} desired*:

From equation A6

$$D_n^2 = \frac{V_{desired} \sqrt{\frac{M_s (T_s + 460)}{P_s}}}{(493.4) C_p (1 - B_{wo}) \sqrt{\Delta P_{ave}}}$$

A5. K factor:

see Derivation Section

$$K = 850 (C_p)^2 (\Delta H @) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2 (D_n)^4$$

A6. Estimated V_{mstd} :

see Derivation Section

$$Est V_{mstd} = (493.4) C_p \sqrt{\frac{P_s}{M_s (460 + T_s)}} \sqrt{P_{ave}} D_n^2 (1 - B_{wo})$$

A7. Estimated V_{meter} reading for entire test or single point

see Derivation Section

$$Est V_m = \frac{(27.98) (T_m + 460)}{Y_d (P_b + \frac{\Delta H}{13.6})} C_p \sqrt{\frac{P_s}{M_s (460 + T_s)}} \sqrt{P_{ave}} D_n^2 (1 - B_{wo})$$

Substitute point values for , H, T_s , and T_m when calculating point volumes.

***A8 Alternate ideal nozzle calculation based on desired ΔH and average ΔP .**

$$Ideal D_n = \frac{\Delta H^{0.25}}{K1 (\Delta P)} = \frac{1.8^{0.25}}{576.80 (0.81)} = 0.2491 \text{ in}$$

Derived from the equation $\Delta H = (\Delta P) K1 (D_n)^4$

K1 is defined on the following page..

Example hand calculation:

1) To simplify calculations, define two intermediate factors - K1 and D1:

$$K1 = 850 (C_p)^2 (\Delta H @) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2$$

$$= 850 (0.84)^2 (1.817) \frac{71 + 460}{459 + 460} \frac{29.605}{29.62} \frac{30.24}{29.59} (1 - 0.053)^2 = 576.80$$

$$D1 = (493.4) C_p \sqrt{\frac{P_s}{M_s (460 + T_s)}} (1 - B_{wo})$$

$$= (493.4) (0.84) \sqrt{\frac{(29.605)}{(29.59)(460 + 459)}} (1 - 0.053) = 12.95$$

2) Find the ideal nozzle size based on the V_{mstd} desired:

$$D_{n \text{ ideal}} = \sqrt{\frac{V_{mstd \text{ desired}}}{D1 \sqrt{P_{ave}}}} = \sqrt{\frac{(30)}{(12.95)(60)(0.90)}} = 0.2071$$

3) Find the closest larger nozzle size and calculate the K factor: (eg. 0.250")

$$K \text{ factor} = K1 (D_{n \text{ actual}})^4 = (576.80) (0.250)^4 = 2.25$$

4) The highest ΔH will be:

$$\Delta H_{\text{highest}} = K (\Delta P_{\text{highest}}) = (2.25) (0.81) = 1.8$$

If ΔH is too high, then reduce D_n to decrease the K factor, and increase the test time to pull the required V_{mstd} .

5) The estimated V_{mstd} will be:

$$V_{mstd} = D1 \sqrt{P_{ave}} D_{n \text{ actual}}^2 = (12.95) (60) (0.90) (0.250)^2 = 43.71$$

Method 5 Results

5

Information required:

	Variable	Example	Units
From the meter card:	H@	1.817	none
Barometric pressure:	P _b	29.62	" Hg
Static pressure of stack:	P _s	-0.20	" H ₂ O
Volume of water collected:	V _{lc}	32	ml
Weight of particulate collected:	M _n	0.040	grams
Test Time:		65.3	minutes
%O ₂ , CO ₂ , N ₂ , CO:	from previous example		
Average H:	H	0.603	"H ₂ O
Pitot tube calibration factor:	C _p	0.84	none
Average meter temp:	T _m	71	°F
Average of P square roots:	√P	0.4068	Root of inches of H ₂ O
Average stack temp:	T _s	459	°F
Volume metered:	V _m	26.94	ft ³
Diameter of nozzle:	D _n	0.276	inches
Area of stack:	A _s	213.72	ft ²
From the meter card:	Y _d	0.9991	none

B1. Volume of water vapor collected, standard:

EPA M5- Eq. 5-2

$$V_{wstd} = (0.04707 \frac{\text{ft}^3}{\text{ml}} @ 68^\circ\text{F}) (V_{lc}) = (0.04707) (32) = 1.5062 \quad 1.51 \text{ scf}$$

B2. Volume of gas metered, standard:

EPA M5- Eq. 5-1

$$V_{mstd} = \frac{(17.64 \frac{^\circ\text{R}}{\text{in. Hg}}) (V_m) P_b + \frac{\bar{H}}{13.6}}{(460 + T_m)} (Y_d)$$

$$= \frac{(17.64) (26.94) 29.62 + \frac{0.603}{13.6}}{(460 + 71)} (0.9991) = 26.5244 \quad 26.52 \text{ dscf}$$

B3. Moisture content:

EPA M5- Eq. 5-3

$$B_{wo} = \frac{V_{wstd}}{V_{mstd} + V_{wstd}} = \frac{1.5062}{26.5244 + 1.5062} = 0.053736 \quad 0.0537 \text{ vol/vol}$$

Note: B_{wo} should also be calculated assuming saturated conditions. See equation F1 on page 15. The lower of the two values should be used (cf. EPA M5- Note 6.5).

M_d, M_s, and P_s are calculated using equations A1, A2, and A3, respectively.

Method 5 Results (Continued)

B4. Velocity of stack gas:

EPA M2- Eq. 2-9

$$V_s = K_p C_p \sqrt{\frac{T_s + 460}{(M_s)(P_s)}} \sqrt{P_{ave}} \quad \text{where } K_p = 85.49 \frac{\text{ft}}{\text{sec}} \sqrt{\frac{(\frac{\text{lb}}{\text{mole}}) \text{in. Hg}}{^\circ\text{R} (\text{in. H}_2\text{O})}}$$

$$= 85.49 (0.84) \sqrt{\frac{459 + 460}{(29.59)(29.605)}} (0.4068) = 29.921 \quad 29.92 \text{ ft/sec}$$

B5. Actual flow of stack gas:

General Equation

$$Q_a = (60 \frac{\text{sec}}{\text{min}}) (A_s) (V_s) = (60) (213.72) (29.921) = 383,683 \quad 383,700 \text{ acfm}$$

B6. Standard stack gas flow:

Derived from EPA M2- Eq. 2-10

$$Q_{std} = \frac{Q_a P_s (17.64 \frac{^\circ\text{R}}{\text{in. Hg}}) (1 - B_{wo})}{T_s + 460}$$

$$= \frac{(383,683) (29.605) (17.64) (1 - 0.053736)}{459 + 460} \quad 206,300 \text{ dscfm}$$

B7. Percent Isokinetic:

EPA M5- Eq. 5-8

$$\%I = \frac{(0.09450) (T_s + 460) V_{mstd}}{P_s V_s A_n (1 - B_{wo})} = \frac{(17.326) (T_s + 460)}{P_s V_s (D_n)^2 (1 - B_{wo})}$$

$$= \frac{(0.09450) (459 + 460) (26.5244)}{(29.605) (29.921) (0.000415475) (65.3) (1 - 0.053736)} = 101.3 \%$$

B8. Particulate Grain Loading:

EPA M5- Eq. 5-6

$$\text{gr/dscf} = \frac{(15.43 \frac{\text{grains}}{\text{gram}}) (M_n)}{V_{mstd}} = \frac{(15.43) (0.040)}{26.5244} = 0.0233$$

Method 6

7

C1. Normality of Titrant:

Dimensional analysis

$$N = \frac{\text{Normality of H}_2\text{SO}_4 \text{ Standard } \frac{\text{meq}}{\text{ml}} (\text{ml H}_2\text{SO}_4 \text{ Standard})}{(\text{ml Titrant})}$$

C2. Concentration (lb/dscf)

EPA M6- Eq. 6-2

$$\text{lb/dscf} = (7.061 \times 10^{-5}) \frac{\text{lb}}{\text{meq}} \times \frac{(V_t - V_{tb}) \frac{\text{ml}}{\text{ml}} N \frac{\text{meq}}{\text{ml}} \frac{V_{\text{soln}} \frac{\text{ml}}{\text{ml}}}{V_a \frac{\text{ml}}{\text{ml}}}}{(V_{\text{mstd}} \frac{\text{dscf}}{\text{dscf}})}$$

See Equation B2 to calculate V_{mstd} .

See Equation E5 and E6 to calculate lb/MBtu.

C3. Conversion of lb/dscf SO₂ to ppm SO₂

Variation of Eq. E2, where MW = 64.06

$$\text{ppm}_{\text{SO}_2} = (\text{lb/dscf}) \cdot 6.015 \times 10^6$$

C4. Audit Concentration Calculation (mg/dscm):

From audit sheet

$$\text{mg/dscm} = 32.03 \frac{\text{mg}}{\text{meq}} \times \frac{(V_t - V_{tb}) \frac{\text{ml}}{\text{ml}} N \frac{\text{meq}}{\text{ml}} \frac{100 \frac{\text{ml}}{\text{ml}}}{V_a \frac{\text{ml}}{\text{ml}}}}{(21 \times 10^{-3} \frac{\text{dscm}}{\text{dscm}})}$$

D1. Drift Calibration:

EPA M6C- Eq. 6C-1

Define:

C_{avg} = Average concentration indicated by the gas analyzer (ppm).

C_o = Average of initial and final system calibration bias check responses for the zero gas (ppm).

C_m = Average of initial and final system calibration bias check responses for the upscale calibration gas (ppm).

C_{ma} = Actual concentration of the upscale calibration gas (ppm).

$$\text{ppm}_{\text{drift calibrated}} = (C_{avg} - C_o) \frac{C_{ma}}{(C_m - C_o)}$$

See Emission Section (page 11) for lb/hr and lb/dscf equations.

D2. Conversion of ppm_{dry} to ppm_{wet}

See proof in Derivation section.

$$\text{ppm}_{\text{wet}} = \text{ppm}_{\text{dry}} (1 - B_{wo})$$

(and for those rare occasions)

D3. Conversion of ppm_{volume basis} to ppm_{mass basis}

$$\text{ppm}_{\text{mass basis}} = \frac{M_p (\text{ppm}_{\text{volume basis}})}{M_d \left(1 - \frac{\text{ppm}_{\text{volume basis}}}{10^6}\right)} \approx \frac{M_p}{M_d} \text{ppm}_{\text{volume basis}}$$

where M_p = molecular weight of the pollutant
 M_d = molecular weight of the stack gas.

The derivation is very similar to that of the conversion of moisture content on a mass/mass basis to vol/vol basis shown in the Derivation Section.

10 Monitors (Continued)

- D4. Standard deviation of the difference between the monitor and the reference method: Appendix B, Spec 2, Eq. 2-2

$$\sigma = \sqrt{\frac{\sum_{i=1}^n d_i^2 - \frac{(\sum_{i=1}^n d_i)^2}{n}}{n-1}} = \sqrt{\frac{\text{sum of (each difference)}^2 - \frac{(\text{sum of all differences})^2}{\text{number of data sets}}}{\text{number of data sets} - 1}}$$

- D5. Confidence coefficient: $t_{0.975}$ table Appendix B, Spec 2, Eq. 2-3, Table 2-1

$$cc = (t_{0.975}) \frac{\sigma}{\sqrt{n}}$$

n	t	n	t	n	t
2	12.706	7	2.447	12	2.201
3	4.303	8	2.365	13	2.179
4	3.182	9	2.306	14	2.160
5	2.776	10	2.262	15	2.145
6	2.571	11	2.228	16	2.131

- D6. Relative Accuracy: Appendix B, Spec 2, Eq. 2-4

$$RA = \frac{|\text{absolute value of the mean of the difference}| + |cc|}{(\text{reference method average or applicable emission standard})} (100)$$

Example:

Run No.	Plant CEM Average	Your Average	Difference	Difference Squared
1	550	560	-10	100
2	455	465	-10	100
3	460	455	5	25
4	490	500	-10	100
5	485	500	-15	225
6	435	450	-15	225
7	500	490	10	100
8	550	530	20	400
9	555	560	-5	25
Average	497.8	501.1	Sum -30	1300

Average of differences = -3.333

$$D4. \quad \sigma = \sqrt{\frac{1300 - \frac{(-30)^2}{9}}{9-1}} = 12.2474$$

$$D5. \quad cc = (2.306) \frac{12.2474}{\sqrt{9}} = 9.4142$$

$$D6. \quad RA = \frac{|-3.333| + |9.4142|}{(501.1)} (100) = 2.5 \%$$

E1. Pounds per hour - particulate:

Dimensional analysis

$$\text{lb/hr} = \frac{(\text{gr/dscf}) (Q_{\text{std}} \frac{\text{dscf}}{\text{min}}) (60 \frac{\text{min}}{\text{hr}})}{7000 \frac{\text{grains}}{\text{lb}}} = \frac{(0.0233) (206,300) (60)}{7000} = 41.2$$

E2. Conversion of ppm (dry basis) to lb/dscf for any gas:

$$\text{lb/dscf} = \frac{(\text{ppm}_{\text{drift calibrated}}) (MW_{\frac{\text{lb}}{\text{mole}}})}{385.3 \frac{\text{dscf}}{\text{lb} \cdot \text{mole}} \times 10^6}$$

Common Molecular Weights

$$\begin{aligned} \text{SO}_2 &= 64.06, \text{ CO} = 28.01 \\ \text{NO}_x &= 46.01, \text{ THC} = 44.10_{(\text{propane})} \end{aligned}$$

Derived from dimensional analysis based on v/v ppm reading. Derivation of molar volume constant can be found in the Derivation section of this manual. Conversion constants for NO_x, SO₂, and CO pre-done in Appendix C.

E3. Pounds per hour from ppm and Q_{std}:

Dimensional analysis

$$\text{lb/hr} = \frac{(\text{ppm}_{\text{drift calibrated}}) (MW_{\frac{\text{lb}}{\text{mole}}}) (Q_{\text{std}} \frac{\text{dscf}}{\text{min}}) (60 \frac{\text{min}}{\text{hr}})}{385.3 \frac{\text{dscf}}{\text{lb} \cdot \text{mole}} \times 10^6}$$

E4. Conversion of lb/dscf or gr/dscf to lb/MBtu for gas or particulate (Fc factor*):

Notice: Pollutant concentration and %CO₂ should be on the same moisture basis EPA M19- Eq. 19-6

$$\text{lb/MBtu} = \frac{(\text{lb/dscf}) (F_c \frac{\text{scf}}{\text{MBtu}}) (100)}{\% \text{CO}_2 (\text{dry basis})} \quad \text{or} \quad \frac{(\text{gr/dscf}) (F_c \frac{\text{scf}}{\text{MBtu}}) (100)}{(7000 \frac{\text{grains}}{\text{lb}}) \% \text{CO}_2 (\text{dry basis})}$$

E5. Conversion of lb/dscf or gr/dscf to lb/MBtu for gas or particulate (Fd factor*):

EPA M20- Eq. 20-6

$$\text{lb/MBtu} = \frac{(\text{lb/dscf}) (F_d \frac{\text{dscf}}{\text{MBtu}}) (20.9)}{(20.9 - \% \text{O}_2)} \quad \text{or} \quad \frac{(\text{gr/dscf}) (F_d \frac{\text{dscf}}{\text{MBtu}}) (20.9)}{(7000 \frac{\text{grains}}{\text{lb}}) (20.9 - \% \text{O}_2)}$$

E6. Calculation of lb/MBtu - heat input method

Dimensional analysis

$$\text{lb/MBtu} = \frac{\text{lb/hr}_{\text{emission}}}{\text{MBtu/hr}_{\text{fired}}}$$

* F_d = 9,780 dscf/MBtu for bituminous coal. See Appendix A for other F_d and F_c factors.

Emissions (Continued)

E7. Correction to a percent CO₂. (eg 12 % CO₂):

EPA M20- Eq. 20-5

$$= \frac{(\text{gr/dscf or lb/dscf}) (\% \text{CO}_2 \text{ correction})}{\% \text{CO}_2 \text{ actual}} \quad \text{eg.} = \frac{(\text{gr/dscf}) (12)}{\% \text{CO}_2}$$

E8. Correction to a percent O₂. (eg 7 % O₂):

EPA M20- Eq. 20-6

$$= \frac{(\text{gr/dscf or lb/dscf}) (20.9 - \% \text{O}_2 \text{ correction})}{(20.9 - \% \text{O}_2 \text{ actual})} \quad \text{eg.} = \frac{(\text{gr/dscf}) (20.9 - 7)}{(20.9 - \% \text{O}_2)}$$

E9. Removal Efficiency for a control device:

General Equation

$$\% = \frac{\text{Inlet} - \text{Outlet}}{\text{Inlet}} (100)$$

E10. Percent Excess Air:

EPA M3B- Eq. 3B-3

$$\% \text{EA} = \frac{\% \text{O}_2 - 0.5 \% \text{CO}}{0.264 \% \text{N}_2 - (\% \text{O}_2 - 0.5 \% \text{CO})}$$

0.264 = Ratio of O₂ to N₂ in air, v/v

Note: The equation above assumes that ambient air is used as the source of O₂ and that the fuel does not contain appreciable amounts of N₂ (as do coke oven or blast furnace gases). For those cases when appreciable amounts of N₂ are present (coal, oil and natural gas do not contain appreciable amounts of N₂) or when oxygen enrichment is used, alternative methods, subject to the approval of the administrator, are required. Reference EPA Method 3B, Section 4.1.

E10.1 Correction to a Percent Excess Air:

similar eq. in 40 CFR 60 Subpart E - 60.54

$$= (\text{lb/dscf}) \frac{100 + \% \text{EA}_{\text{actual}}}{100 + \% \text{EA}_{\text{correction}}}$$

E11. Pounds per 1000 pounds stack gas: Dimensional analysis and intuition:

$$= \frac{(M_n^{\text{grams}}) \frac{1}{453.59} \frac{\text{lb}}{\text{grams}}}{(V_{\text{mstd}}^{\text{ft}^3}) 2.595 \times 10^{-3} \frac{\text{lb} \cdot \text{mole}}{\text{ft}^3} (M_d \frac{\text{lb}}{\text{lb} \cdot \text{mole}}) + (V_{\text{lc}}^{\text{ml}}) (2.205 \times 10^{-3} \frac{\text{lbs}}{\text{ml}})} \times 1000$$

2.595 x 10⁻³ is n/V=P/RT from the ideal gas law.

2.205 x 10⁻³ assumes 1 ml of water = 1 gram.

Corrections for Soot Blowing Information required

E_s	Average lb/Mbtu of particulate for soot blowing runs
E_{ns}	Average lb/Mbtu of particulate for non-soot blowing runs
A	Hours of soot-blowing during test runs containing soot blowing
B	Hours not soot blowing during test runs containing soot blowing
R	Average hours of boiler operation per 24 hour day
S	Average hours of soot blowing per 24 hour day

E12. Weighted average for all runs: Wisconsin Administrative Code DNR: NR 439.07 (8)

$$E_{avg} = E_s \frac{(A + B) \cdot S}{(A \cdot R)} + E_{ns} \frac{(R \cdot S)}{R} - \frac{B \cdot S}{A \cdot R}$$

Example

Company XXX runs their boiler 24 hours per day. They blow soot for five minutes, three times per day. Three particulate runs were performed. The results were as follows:

Soot Blowing Runs			Non Soot Blowing Runs		
Run#	Run Time	lb/MBtu	Run#	Run Time	lb/MBtu
1	60 min	0.4000	3	60 min	0.3000
2	72 min	0.5000			

$$E_s = \frac{(0.5000 + 0.4000)}{2} = 0.4500 \text{ lb/MBtu} \quad E_{ns} = 0.3000 \text{ lb/MBtu}$$

$$A = \frac{(5 + 5) \text{ min}}{60 \frac{\text{min}}{\text{hr}}} = 0.1667 \text{ hr} \quad B = \frac{(72 + 60 - 5 - 5) \text{ min}}{60 \frac{\text{min}}{\text{hr}}} = 2.0333 \text{ hr}$$

$$R = 24 \text{ hr} \quad S = \frac{(3 \times 5) \text{ min}}{60 \frac{\text{min}}{\text{hr}}} = 0.25 \text{ hr}$$

$$E_{avg} = 0.4500 \frac{(0.1667 + 2.0333) \times 0.25}{(0.1667 \times 24)} + 0.3000 \frac{(24 - 0.25)}{24} - \frac{2.0333 \times 0.25}{0.1667 \times 24}$$

$$= 0.06186 + 0.25875 = 0.3206 \text{ lb/MBtu}$$

The weighted average for all three runs is 0.3206 lb/MBtu.

F1. Moisture content, assuming saturated conditions:

Calculate the absolute stack pressure P_s , and look in Appendix F to find the saturated vapor pressure (SVP) at the average stack temperature. Calculate the saturated moisture content as follows:

$$B_{wo} = \frac{\text{svp @ } T_s}{P_s}$$

If $P_s = 30.5$ "Hg and $T_s = 140^\circ\text{F}$, then $\text{svp @ } T_s = 5.879$

$$B_{wo} = \frac{5.879}{30.5} = 0.1928$$

Best used if P_s does not deviate from more than 1 in Hg from standard conditions.

F2. Ambient Conditions:

(EPA M19 - Section 2.2.1.1)

$$B_{wo} = 0.027$$

$$M_d = 28.84$$

Assuming:

$$\begin{aligned} \%N_2 &= 78.2\% \\ \%O_2 &= 20.9 \\ \%CO &= 0.0 \\ \%CO &= 0.0 \end{aligned}$$

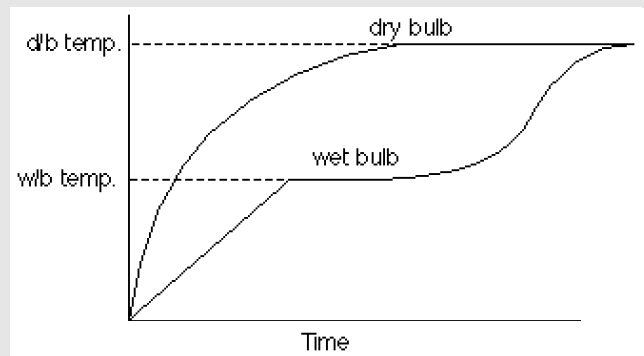
Note: The above assumption does not consider argon in air (about 0.9 percent, molecular weight of 39.9). A negative error of 0.4 percent is introduced. The tester may choose to include argon in the analysis using procedures subject to the approval of the administrator. EPA M3- Section. 7.1.

Moisture Determination (Bwo) Using Wet Bulb/ Dry Bulb Method

Information required:	Variable	Example	Units
Static Pressure of Stack:	P_{static}	-0.20	" H ₂ O
Barometric Pressure:	P_b	29.62	" Hg
Wet Bulb Temperature:	t_w	77	°F
Dry Bulb Temperature:	t_d	100	°F

Obtain the Wet and Dry Bulb Temperatures

The graph below illustrates how the temperature changes when a wet bulb is placed in an air stream. The temperature reaches equilibrium at the wet bulb temperature and then continues to rise as the water on the bulb dries. Above around 130°F, the moisture on the bulb dries too quickly to determine the stabilized temperature. Also, the stack gas velocity should be at least 10 ft/sec to acquire an accurate reading.



State of Oregon

The dry bulb temperature is the normal temperature measured by a dry thermometer.

Calculate the absolute stack pressure using equation A1:

$$P_s = P_b + \frac{P_{\text{static}} \frac{\text{H}_2\text{O}}{\text{Hg}}}{13.6 \frac{\text{H}_2\text{O}}{\text{Hg}}} = 29.62 + \frac{-0.20}{13.6} = 29.605 \text{ inches Hg}$$

Determine B_{wo} using a Psychrometric chart or Vapor Pressure Tables

By Psychrometric Chart:

Using the Psychrometric chart in the back of this manual locate the dry bulb temperature on the x-axis and the wet bulb temperature along the curved saturation line. From their intersection read directly left to the y-axis to find the humidity, H , in pounds water per pounds bone dry air. Convert H to B_{wo} with the following equation.

(Eg. If $t_w = 77$ and $t_d = 100$, then $H = 0.01475$ lb water/ lb bone dry air.)

F3. Conversion of lb/lb moisture content (H) to B_{wo}

see Derivation Section

$$B_{wo} = \frac{H M_d}{H M_d + 18.01} \quad (v/v)$$

$$= \frac{(0.01475)(28.84)}{(0.01475)(28.84) + 18} \approx 0.0231$$

$M_d = 28.84$
for ambient
conditions.

The psychrometric chart is based on a standard barometric pressure of 29.92 in. Hg. If the absolute stack pressure deviates significantly from standard conditions the result must be corrected (which is beyond the present scope of this manual).

Moisture Determination (B_{wo})

Using Wet Bulb/ Dry Bulb Method (Continued)

By Vapor Pressure Table:

Nomenclature:

Saturated Vapor Pressure: s.v.p.

Vapor Pressure: v.p.

Find the saturated vapor pressure (s.v.p) from the vapor pressure table in Appendix E, based on the wet bulb temperature (t_w):

Eg. s.v.p @ 77 °F = 0.9352 in. Hg

F4. Calculate the actual vapor pressure (v.p.): (temperatures are in °F)

$$\begin{aligned} \text{v.p.} &= \text{s.v.p. if } t_d = t_w \\ \text{else v.p.} &= \text{s.v.p.} - (3.67 \times 10^{-4}) (P_s) (t_d - t_w) \left(1 + \frac{t_w - 32}{1571} \right) \end{aligned}$$

$$\text{v.p.} = 0.9352 - (3.67 \times 10^{-4}) (29.605) (100 - 77) \left(1 + \frac{77 - 32}{1571} \right) = 0.67815 \text{ in. Hg}$$

If P_s is below 29.5 in. Hg. the QAH, Section 3.12, for EPA Method 9 uses a constant of 3.57×10^{-4} in place of 3.67×10^{-4} .

F4.1 Relative Humidity

Calculate the relative humidity by dividing the v.p. calculated in equation F4, by the s.v.p. at the **dry** bulb temperature.

F5. Calculate B_{wo} :

$$B_{wo} = \frac{\text{v.p.}}{P_s} \quad B_{wo} = \frac{0.67815}{29.605} = .0229$$

F6. If no vapor pressure table is available, the vapor pressure for a given wet bulb temperature can be found from the follow equation:

$$\begin{aligned} \text{s.v.p.} = & 0.0375 + 0.2103 T_1 + 0.28665 T_2 + 0.17595 T_3 \\ & + 0.04615417 T_4 + 0.00452083 T_5 \end{aligned}$$

where:

$$T_1 = t_w / 40; \quad T_2 = T_1 (T_1 - 1); \quad T_3 = T_2 (T_1 - 2); \quad T_4 = T_3 (T_1 - 3); \quad T_5 = T_4 (T_1 - 4)$$

Critical Orifice Check

A critical orifice can be used to check the calibration on a dry gas meter. Each orifice has two parameters: the orifice coefficient, K' ; and the critical vacuum. Above the critical vacuum, only a fixed rate of molecules are allowed to enter the dry gas meter.

Check the meter calibration as follows:

- Turn the meter on and let it run for about 15 minutes to let it warm up and stabilize the temperature inside.
- Attach the critical orifice (quick-connect) and crank up the meter to get the highest possible flow rate.
- While the meter is running start your watch and read the starting volume on the fly.
- Run the meter for fifteen minutes, taking volume readings on the fly every five minutes. Be sure to record the meter temperatures as well as the ambient temperature near the critical orifice. Each five minute interval can be considered a separate trial.

Calculations:

Calculate the V_{mstd} as normal using equation B2.

$$V_{mstd} = \frac{(17.64 \frac{^{\circ}R}{in. Hg}) (V_m) P_b + \frac{\bar{H}}{13.6} (Y_d)}{(460 + T_m)}$$

Calculate the volume drawn through the orifice.

G1. Critical Orifice Volume:

EPA M5 - Eq. 5-11

$$V_{or std} = \frac{P_b (\text{elapsed time}) (K')}{\sqrt{T_{amb} + 460}}$$

$$\text{where } K' = \text{is the orifice coefficient} = \frac{ft^3 \sqrt{^{\circ}R}}{(in. Hg) (min)}$$

and T_{amb} = ambient temperature

Calculate the percent difference.

G2. Percent Difference:

$$\% \text{ Diff} = \frac{(V_{mstd} - V_{or std})}{V_{or std}} \times 100$$

Miscellaneous (Continued)

G3. To find barometric pressure at your altitude given barometric at sea level:

$$\begin{aligned}
 \text{B.P. @ Altitude} &= \text{B.P. @ sealevel} - \frac{0.075 \frac{\text{lb air}}{\text{ft}^3} \text{ density of air} (\text{Altitude}) (29.92 \text{ in. Hg})_{\text{std Pb @ sea level}}}{144 \frac{\text{in}^2}{\text{ft}^2} \quad 14.7 \frac{\text{lb}}{\text{ft}^2} \text{ standard pressure @ sea level}} \\
 &= \text{B.P. @ sealevel} - (\text{Altitude}) 0.001060 \frac{\text{in. Hg}}{\text{ft}}
 \end{aligned}$$

Commonly Used Constants

17.64 Combination of standard barometric pressure and temperature: EPA M5- Eq. 5-1

$$17.64 = \frac{T_{std}}{P_{std}} = \frac{527.67 \text{ }^{\circ}\text{R}}{29.921 \text{ in. Hg}}$$

85.49 Velocity constant Kp*:

EPA M2- Section 5.1, 5.2

$$K_p = \sqrt{2 (\rho) (g) (R)}$$

where ρ = density of water $\frac{\text{lb}}{\text{ft}^3}$
 g = gravitational constant $\frac{\text{ft}}{\text{sec}^2}$
 R = ideal gas law constant $\frac{\text{in. Hg ft}^3}{\text{lb} \cdot \text{mole } ^{\circ}\text{R}}$

$$= \sqrt{\frac{2 (62.428) \frac{\text{lb}}{\text{ft}^3} (32.174) \frac{\text{ft}}{\text{sec}^2} (21.83) \frac{\text{in. Hg ft}^3}{\text{lb} \cdot \text{mole } ^{\circ}\text{R}}}{12 \frac{\text{in}}{\text{ft}}}}$$

$$= 85.4857 \frac{\text{ft}}{\text{sec}} \sqrt{\frac{\text{lb}}{\text{lb} \cdot \text{mole } ^{\circ}\text{R}} \frac{(\text{in. Hg})}{(^{\circ}\text{R})(\text{in. H}_2\text{O})}} \approx 85.49$$

The derivation of this constant was taken from the SSPP Student Manual Appendix C and uses a gas constant (R) of 21.83 which differs from the PH value of 21.85. Nonetheless, Kp = 85.49 is used in EPA M2- Eq. 2.9.

385.3 Molar volume of 1 lb•mole of air at STP:

Where $P_{std} = 1 \text{ atm} = 29.921 \text{ in. Hg}$
 $T_{std} = 68^{\circ} \text{ F} = 527.67 \text{ }^{\circ}\text{R}$
 $R = 21.85 \frac{\text{in. Hg ft}^3}{\text{lb} \cdot \text{mole } ^{\circ}\text{R}}$

From $PV = nRT$ ideal gas law

$$\frac{V}{n} = \frac{RT}{P} = \frac{(21.85) \frac{\text{in. Hg ft}^3}{\text{lb} \cdot \text{mole } ^{\circ}\text{R}} (527.67) ^{\circ}\text{R}}{(29.921) \text{ in. Hg}} = 385.3 \frac{\text{dscf}}{\text{lb} \cdot \text{mole}}$$

Derivations (Continued)

Derivation of $\text{ppm}_{\text{wet}} = \text{ppm}_{\text{dry}} (1 - B_{\text{wo}})$:

Define

V_{pol} = Volume of pollutant

V_{dry} = Volume of dry air

V_{vap} = Volume of water vapor

By Definition

$$\text{ppm}_{\text{dry}} = \frac{V_{\text{pol}}}{V_{\text{dry}} \times 10^6}$$

$$\text{ppm}_{\text{wet}} = \frac{V_{\text{pol}}}{V_{\text{dry}} + V_{\text{vap}} \times 10^6}$$

$$B_{\text{wo}} = \frac{V_{\text{vap}}}{V_{\text{dry}} + V_{\text{vap}}}$$

Therefore

$$1 - B_{\text{wo}} = \frac{V_{\text{dry}} + V_{\text{vap}}}{V_{\text{dry}} + V_{\text{vap}}} - \frac{V_{\text{vap}}}{V_{\text{dry}} + V_{\text{vap}}}$$

$$= \frac{V_{\text{dry}}}{V_{\text{dry}} + V_{\text{vap}}}$$

$$\begin{aligned} \text{ppm}_{\text{dry}} (1 - B_{\text{wo}}) &= \frac{V_{\text{pol}}}{V_{\text{dry}} \times 10^6} \times \frac{V_{\text{dry}}}{V_{\text{dry}} + V_{\text{vap}}} \\ &= \frac{V_{\text{pol}}}{V_{\text{dry}} + V_{\text{vap}} \times 10^6} \\ &= \text{ppm}_{\text{wet}} \end{aligned}$$

QED

Moisture Content Conversion

Derivation of the conversion of the moisture content measured on a mass/mass basis to a volume/volume basis and vice versa.

Define:

H = humidity (kg/kg or lb/lb)

m_w = mass of water

n_w = moles of water

M_d = molecular weight of air

B_{wo} = moisture content (vol/vol)

m_a = mass of air

n_a = moles of air

Convert mass to moles:

$$H \frac{\text{kg water}}{\text{kg air}} \times \frac{\text{kg} \cdot \text{mole of water}}{18 \text{ kg water}} \times \frac{M_d \text{ kg}}{\text{kg} \cdot \text{mole of air}} = \frac{n_w}{n_a}$$

$$\frac{H M_d}{18} = \frac{n_w}{n_a}$$

Invert:
$$\frac{18}{H M_d} = \frac{n_a}{n_w} \quad (A)$$

Convert volume to moles:
(Ideal gas law with T and P constant)

$$B_{wo} = \frac{V_{\text{vap}}}{V_{\text{vap}} + V_{\text{dry}}} = \frac{n_w}{n_w + n_a}$$

Invert:
$$\frac{1}{B_{wo}} = \frac{n_w + n_a}{n_w}$$

$$\frac{1}{B_{wo}} = 1 + \frac{n_a}{n_w} \quad (B)$$

Substitute equation A into B:

$$\frac{1}{B_{wo}} = 1 + \frac{18}{H M_d}$$

Rearrange to solve for B_{wo} and H:

$$B_{wo} = \frac{H M_d}{H M_d + 18} \quad (v/v)$$

$$H = \frac{18 (B_{wo})}{M_d (1 - B_{wo})} \quad (\text{mass/mass})$$

Derivations (Continued)

K Factor Equations

There are three sources for the K factor equation. The final is a compromise whose constant more closely reflects the SSPP Student Manual and the EPA spreadsheet. Each equation's impact on the final K factor is shown.

- 1) The generally accepted CAE equation:

$$K = 2.89 \times 10^7 (C_p)^2 (\Delta H@) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2 (A_n)^2$$

Substituting $A_n = \pi \frac{D_n^2}{24}$ yields:

$$K = 859.7 (C_p)^2 (\Delta H@) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2 (D_n)^4$$

Using the example numbers in on page 1:

$$K = 859.7 (0.84)^2 (1.817) \frac{71 + 460}{459 + 460} \frac{29.605}{29.62} \frac{30.24}{29.59} (1 - 0.053)^2 (0.25)^4 = 2.28$$

- 2) The SSPP Student Manual:

$$K = 846.72 (C_p)^2 (\Delta H@) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2 (D_n)^4 = 2.24$$

- 3) An EPA spreadsheet from the EMTIC bulletin board by Bob McCracken:

$$K = 846.872 (C_p)^2 (\Delta H@) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b + \frac{\Delta H@}{13.6}} \frac{M_d}{M_s} (1 - B_{wo})^2 (D_n)^4 = 2.23$$

Final Equation:

$$K = 850 (C_p)^2 (\Delta H@) \frac{T_m + 460}{T_s + 460} \frac{P_s}{P_b} \frac{M_d}{M_s} (1 - B_{wo})^2 (D_n)^4 = 2.25$$

Estimated Volume Metered at Standard Conditions

The equation assumes isokinetic conditions. The volume is calculated from the flow through the nozzle and is corrected to dry standard conditions.

Define:

V_{mstd} = Volume metered at standard conditions	T_{std} = Standard temperature (527.67 °R)
Q_{nozzle} = flow rate through nozzle (ft ³ /min)	T_s = Temperature of stack (°R)
= Total test time (min)	P_{std} = Standard pressure (29.921 "Hg)
B_{wo} = Moisture content (vol/vol)	P_s = Absolute stack pressure ("Hg)
A_n = Area of nozzle (ft ²)	D_n = Diameter of nozzle (inches)
V_s = Velocity of stack gas (ft/sec)	C_p = Pitot coefficient (0.84 for S-Type)
M_s = Molecular weight of stack gas	
$\sqrt{P_{ave}}$ = Average of the square root delta P's	

Basic equation:

$$V_{mstd} = Q_{nozzle} \frac{ft^3}{min} \min \frac{T_{std}}{T_s} \frac{P_s}{P_{std}} (1 - B_{wo})$$

Substitute Q=VA:

$$= (V_{s \frac{ft}{sec}}) A_n \frac{ft^2}{(60 \frac{sec}{min})} \min \frac{T_{std}}{T_s} \frac{P_s}{P_{std}} (1 - B_{wo})$$

Substitute for Vs and An: $V_s = 85.49 C_p \sqrt{\frac{T_s}{M_s P_s}} \sqrt{P_{ave}} A_n = \pi \frac{D_n^2}{24}$

$$= 85.49 C_p \sqrt{\frac{T_s}{M_s P_s}} \sqrt{P_{ave}} \frac{ft}{sec} \pi \frac{D_n^2}{24} (60 \frac{sec}{min}) \min \frac{T_{std}}{T_s} \frac{P_s}{P_{std}} (1 - B_{wo})$$

Combine constants and like terms:

$$= \frac{(85.49)(60)\pi(527.67)}{(24)^2(29.921)} C_p \sqrt{\frac{T_s}{M_s P_s}} \frac{P_s}{T_s} \sqrt{P_{ave}} D_n^2 (1 - B_{wo})$$

Reduce:

$$Est V_{mstd} \approx (493.4) C_p \sqrt{\frac{P_s}{M_s T_s}} \sqrt{P_{ave}} D_n^2 (1 - B_{wo})$$

Estimated actual volume meter reading:

To determine the volume meter reading (ie. at meter conditions) substitute the meter temperature, T_m (°F) + 460, for T_{std} and the meter pressure, P_m , for P_{std} and divide by Y_d .

$$Est V_m \approx \frac{(27.98)(T_m + 460)}{Y_d (P_b + \frac{\Delta H}{13.6})} C_p \sqrt{\frac{P_s}{M_s T_s}} \sqrt{\Delta P_{ave}} D_n^2 (1 - B_{wo})$$

where $P_m = P_b + \frac{H}{13.6}$

Appendix A

Fc and Fd Factors

27

AA1. Calculation of F_d factor from fuel analysis (as received basis)

EPA M19- Eq. 19-13

$$F_d = \frac{(3.64) \%H_2 + (1.53) \%C + (0.57) \%S + (0.14) \%N - (0.46) \%O_2 \frac{\text{scf}}{\text{lb}} \cdot 10^6 \frac{\text{Btu}}{\text{MBtu}}}{GCV \frac{\text{Btu}}{\text{lb}}}$$

AA2. Calculation of F_c factor from fuel analysis (as received basis)

EPA M19- Eq. 19-14

$$F_c = \frac{(0.321) \%C \frac{\text{scf}}{\text{lb}} \cdot 10^6 \frac{\text{Btu}}{\text{MBtu}}}{GCV \frac{\text{Btu}}{\text{lb}}}$$

Percent H_2 , C, S, N, and O_2 taken from **Ultimate** coal analysis.

F Factors for Various Fuels

EPA M19, Table 19-1

Fuel Type	F_d dscf/MBtu	F_w wscf/MBtu	F_c scf/MBtu
Coal:			
Anthracite.....	10,100	10,540	1,970
Bituminous	9,780	10,640	1,800
Lignite.....	9,860	11,950	1,910
Oil	9,190	10,320	1,420
Gas:			
Natural.....	8,710	10,610	1,040
Propane.....	8,710	10,200	1,190
Butane.....	8,710	10,390	1,250
Wood	9,240		1,830
Wood Bark.....	9,600		1,920
Municipal	9,570		1,820

Appendix B

Blank Residue Limits

SOLVENT	DENSITY	VOLUME OF BLANK					
		50 ml	100 ml	150 ml	200 ml	250 ml	500 ml
ACETONE	0.7857	0.0004	0.0008	0.0012	0.0016	0.0020	0.0039
BENZENE	0.8787	0.0004	0.0009	0.0013	0.0018	0.0022	0.0044
CHLOROFORM	1.4832	0.0007	0.0015	0.0022	0.0030	0.0037	0.0074
ETHYL ETHER	0.7138	0.0004	0.0007	0.0011	0.0014	0.0018	0.0036
HEXANE	0.6603	0.0003	0.0007	0.0010	0.0013	0.0017	0.0033
2-PROPANOL	0.7855	0.0004	0.0008	0.0012	0.0016	0.0020	0.0039
METHANOL	0.7914	0.0004	0.0008	0.0012	0.0016	0.0020	0.0040
METHYLENE CHLORIDE	1.3266	0.0007	0.0013	0.0020	0.0027	0.0033	0.0066
TOLUENE	0.8669	0.0004	0.0009	0.0013	0.0017	0.0022	0.0043
WATER	1.0000	0.0005	0.0010	0.0015	0.0020	0.0025	0.0050

RESIDUE IN GRAMS

The maximum allowable blank for acetone used for an EPA M5 test is 0.001 percent of the acetone weight. (EPA M5- Section 3.2) The same criteria is used for Methylene Chloride in EPA M202.

To calculate the allowable blank residue weight for other solution volumes, divide the density by 100,000 (0.001 percent), then multiple by the new volume. Do all calculations first, then round the final value to four decimal places, which is the accuracy of the analytical balance.

$$\text{Limit on liquid blank} = (\text{Liquid Density g/ml}) * (\text{Volume ml}) * (0.001)/100$$

The density of acetone was taken from its VWR Scientific container. All other densities were taken from the CRC Handbook of Chemistry, 56th Edition, 1975 - 1976.

Note for Backhalf water condensibles:

For backhalf water condensibles, subtract V_{lc} from the total (sample collected plus the rinse). Use this volume when calculating allowable blank value.

Length		Velocity			
1 cm	=	0.3937	in	1 m/s	= 3.2808 ft/s
1 m	=	3.2808	ft	1 mph	= 1.4667 ft/s
1 yd	=	3	ft	1 mph	= 0.8684 knot
1 mi	=	5280	ft	1 km/h	= 0.27778 m/s
1 km	=	3280.8	ft	1 km/h	= 0.62138 mph
Pressure			Area		
1 "Hg	=	33.864 mbar	1 cm ²	=	0.15500 in ²
1 atm	=	29.921 "Hg	1 m ²	=	10.76391 ft ²
1 atm	=	1013.25 mbar	1 mi ²	=	2.5899 m ²
1 atm	=	760 mm Hg	1 yd ²	=	0.8361274 m ²
1 atm	=	14.696 psi	1 acre	=	4074 m ²
1 psi	=	2.036 "Hg	1 acre	=	43,560 ft ²
1 psi	=	6.895 kPa	1 mi ²	=	2.5900 km ²
Volume			Mass		
1 ft ³	=	28.316 liter	1 oz	=	28.350 g
1 liter	=	0.03532 ft ³	1 lb	=	0.45359 kg
1 liter	=	0.26418 gal	1 kg	=	2.2046 lb
1 m ³	=	264.18 gal	1 g	=	15.432 grains
1 ft ³	=	7.4806 gal	1 lb	=	7000 grains
1 m ³	=	35.314 ft ³	1 kip	=	1000 lb
1 in ³	=	16.3871 cm ³			
Volume Flow Rate			Temperature		
1 cfm	=	7.4805 gal/min	°F	=	(9/5)•°C + 32
1 cfm	=	0.4719 liter/s	°R	=	°F + 459.67
1 m ³ /s	=	35.316 ft ³ /s	°C	=	5/9•(°F - 32)
1 m ³ /s	=	2119 cfm	°K	=	°C + 273.15
1 gal/min	=	0.13368 cfm	°K	=	(5/9)•(°F - 32) + 273
Work and Heat			Power		
1 Btu	=	777.65 ft-lb	1 Hp	=	550.00 ft-lb/s
1 Btu	=	1054.3 J	1 Hp	=	2545.5 Btu/hr
1 Btu	=	0.292875 W-hr	1 Hp	=	745.70 W
1 J	=	9.4845 x 10 ⁻⁴ Btu	1 W	=	3.4135 Btu/hr
1 J	=	107 ergs	1 kW	=	1.3410 Hp
1 kW-hr	=	3414.4 Btu			
1 Cal	=	3.0860 ft-lb			
Gas Concentration Conversions:					
1 lb/scf	=	(ppm SO ₂) (1.660 x 10 ⁻⁷) or	EPA M19 - Section 2		
	=	(ppm NO _x) (1.194 x 10 ⁻⁷) or	EPA M19 - Section 2		
	=	(ppm CO) (7.270 x 10 ⁻⁸)	From Equation E2		

Common Molecular Weights

SO₂ = 64.06, CO = 28.01NO_x = 46.01, THC = 44.10 (propane)

Appendix D

Shipping Information

Air Freight	Phone #	Account #
SEKO	1-800-323-1964	414824
American	1-800-334-7400	F639370
Continental	1-312-686-4720	235546
Fed Ex	1-800-238-5355	0605-1738-0
Northwest	1-800-692-2746	433440
TWA	1-800-892-6398	STL 1472015
United	1-800-631-1500	362655
US Air	1-312-686-7150	C 493710

General Notes on Shipping:

The shipper will want to know the number of packages being shipped and the total weight. Label each box as # ____ of ____ (eg # 5 of 25). Clean Air Shipping labels are generally acceptable.

Be sure to clear it with the client in terms of where the goods may be left for pickup (eg. do they have a shipping and receiving building.)

Saturated Vapor Pressure Table

Temperature (T) in °F and SVP in "Hg

T	SVP	T	SVP	T	SVP	T	SVP	T	SVP
30	0.1647	67	0.6669	104	2.178	141	6.032	178	14.62
31	0.1715	68	0.6903	105	2.243	142	6.188	179	14.95
32	0.1803	69	0.7144	106	2.310	143	6.348	180	15.29
33	0.1878	70	0.7392	107	2.379	144	6.511	181	15.63
34	0.1955	71	0.7648	108	2.449	145	6.678	182	15.98
35	0.2035	72	0.7912	109	2.521	146	6.848	183	16.33
36	0.2118	73	0.8183	110	2.596	147	7.022	184	16.69
37	0.2203	74	0.8462	111	2.672	148	7.200	185	17.06
38	0.2292	75	0.8750	112	2.749	149	7.382	186	17.44
39	0.2383	76	0.9046	113	2.829	150	7.567	187	17.82
40	0.2478	77	0.9352	114	2.911	151	7.756	188	18.21
41	0.2576	78	0.9666	115	2.995	152	7.950	189	18.60
42	0.2677	79	0.9989	116	3.081	153	8.147	190	19.01
43	0.2783	80	1.032	117	3.169	154	8.349	191	19.42
44	0.2891	81	1.066	118	3.259	155	8.554	192	19.84
45	0.3004	82	1.102	119	3.351	156	8.765	193	20.26
46	0.3120	83	1.138	120	3.446	157	8.979	194	20.70
47	0.3240	84	1.175	121	3.543	158	9.198	195	21.14
48	0.3364	85	1.213	122	3.642	159	9.421	196	21.59
49	0.3493	86	1.253	123	3.744	160	9.649	197	22.04
50	0.3626	87	1.293	124	3.848	161	9.882	198	22.51
51	0.3764	88	1.335	125	3.954	162	10.12	199	22.98
52	0.3906	89	1.378	126	4.063	163	10.36	200	23.46
53	0.4052	90	1.422	127	4.174	164	10.61	201	23.95
54	0.4203	91	1.467	128	4.289	165	10.86	202	24.45
55	0.4359	92	1.513	129	4.406	166	11.12	203	24.95
56	0.4520	93	1.561	130	4.525	167	11.38	204	25.47
57	0.4586	94	1.610	131	4.647	168	11.65	205	25.99
58	0.4858	95	1.660	132	4.772	169	11.92	206	26.53
59	0.5035	96	1.712	133	4.900	170	12.20	207	27.07
60	0.5218	97	1.765	134	5.031	171	12.48	208	27.62
61	0.5407	98	1.819	135	5.165	172	12.77	209	28.18
62	0.5601	99	1.875	136	5.302	173	13.06	210	28.75
63	0.5802	100	1.932	137	5.442	174	13.36	211	29.33
64	0.6009	101	1.992	138	5.585	175	13.67	212	29.92
65	0.6222	102	2.052	139	5.732	176	13.98		
66	0.6442	103	2.114	140	5.879	177	14.30		

SVP values for temperatures ranging from 30 to 139°F were taken from the Quality Assurance Handbook for Air Pollution Measurement Systems: Volume III., Stationary Source Specific Methods, Addition Section 3.12, Method 9 - Visible Determination of Opacity Emissions from Stationary Sources, Table 6.2.

High temperatures were approximated from polynomial F6 shown on page 17 based on empirical data.

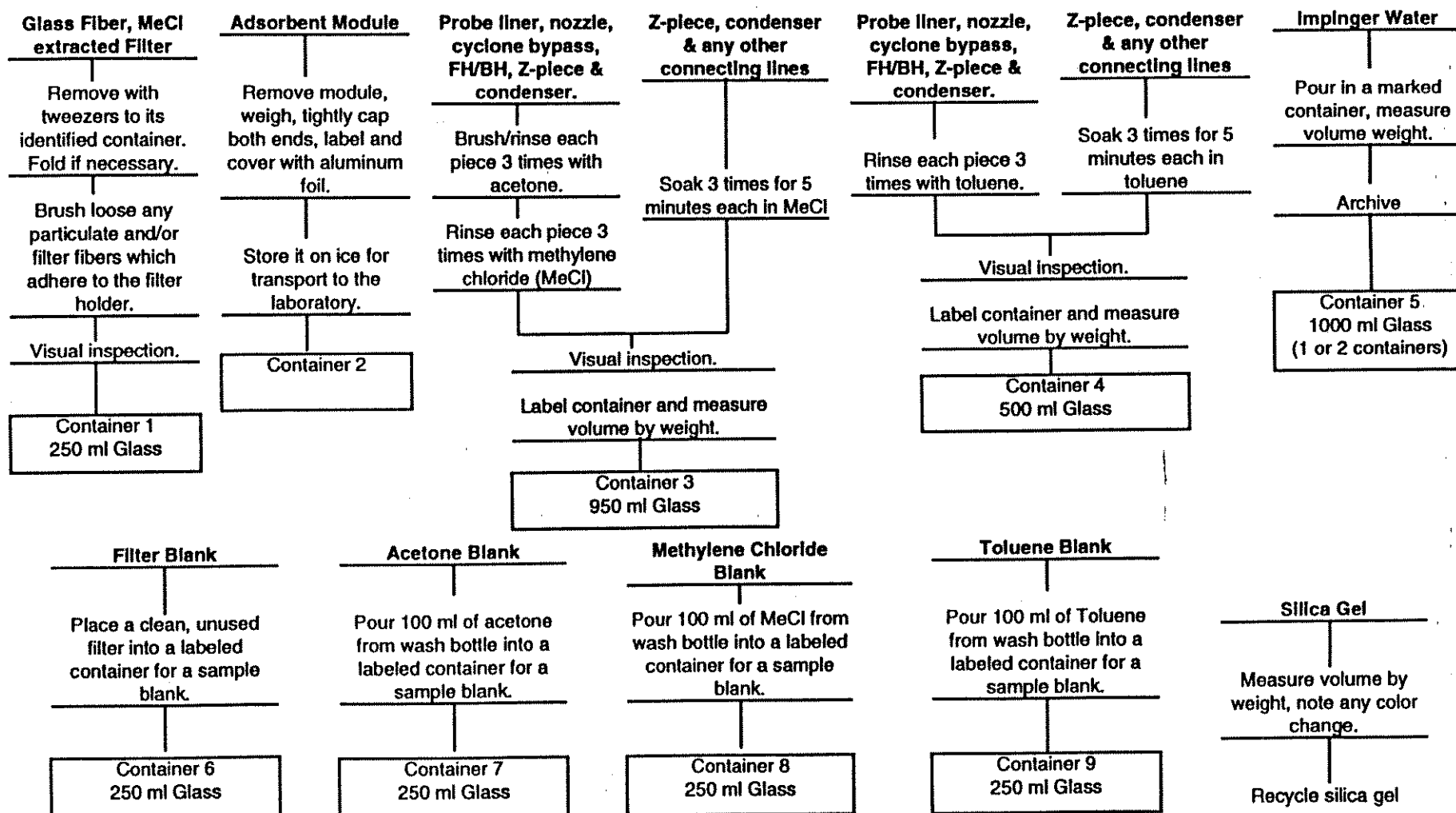
CLEAN AIR ENGINEERING

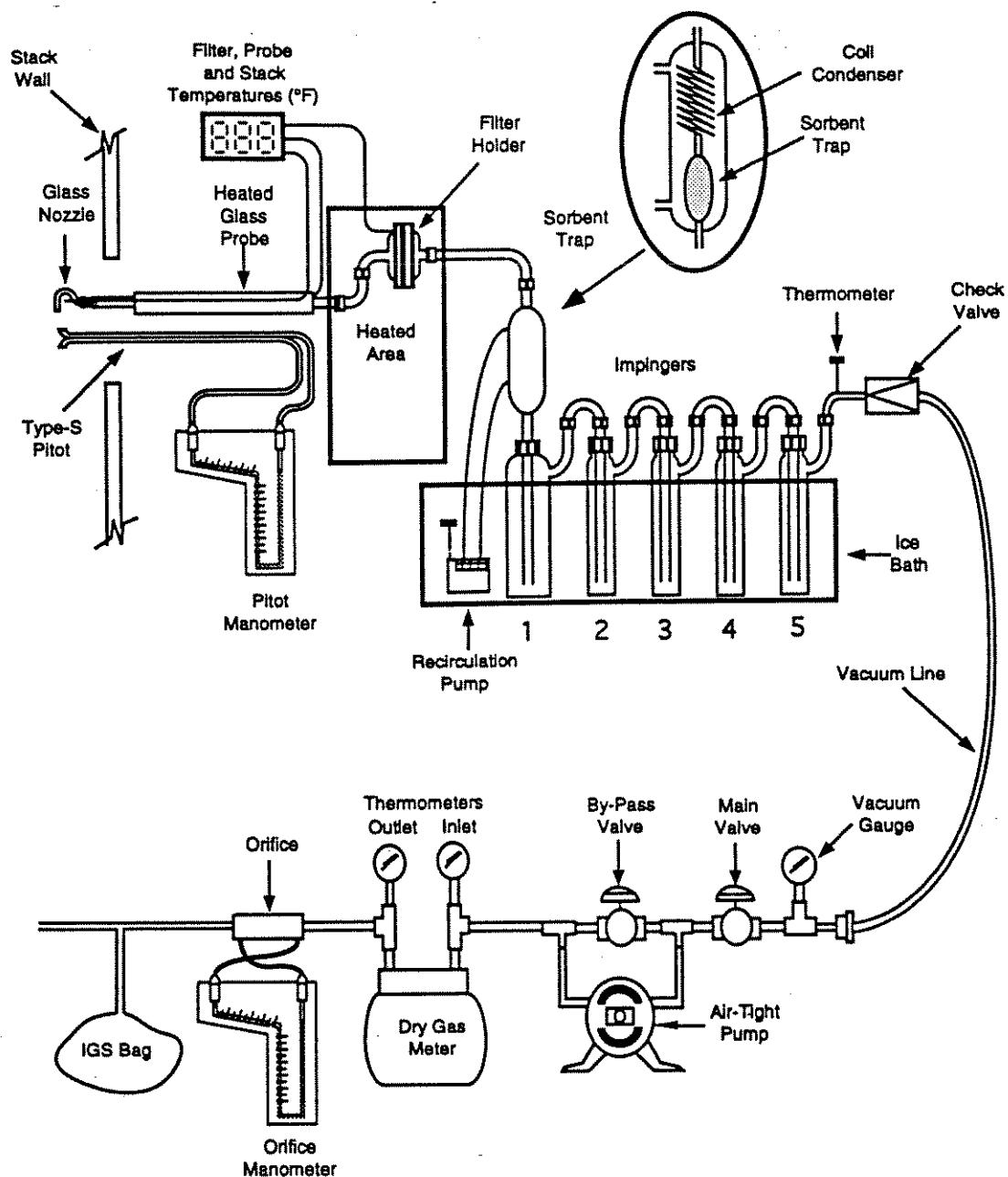
SAMPLING RECOVERIES AND TRAINS

REVISION 0: NOVEMBER 10, 1995

METHOD 23 - DETERMINATION OF POLYCHLORINATED DIBENZO-P-DIOXINS AND POLYCHLORINATED DIBENZOFURANS EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M23 - Dioxins/Furans

Impinger 1	empty
Impinger 2	100 ml HPLC water
Impinger 3	100 ml HPLC water
Impinger 4	empty
Impinger 5	silica gel

METHOD 12 - DETERMINATION OF INORGANIC LEAD EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Unweighed, Gelman Filter

Remove with tweezers to its identified container.
Fold if necessary.

Brush loose any particulate and/or filter fibers which adhere.

Visual inspection.

Container 1
Petri Dish

Probe liner, nozzle, cyclone bypass, and filter front half (FH).

Brush/rinse 3 times with 0.1 N HNO₃.

Visual inspection.

Label container and measure volume by weight.

Container 2
250 ml Plastic

Back half (BH) filter housing, Z-piece, impingers 1,2,3 and U-bends

Measure volume by weight.

Empty contents into labeled container.

Clean each piece 3 times with 0.1 N HNO₃.

Visual inspection.

Label container and measure volume by weight.

Container 3
1000 ml Plastic

Filter Blank

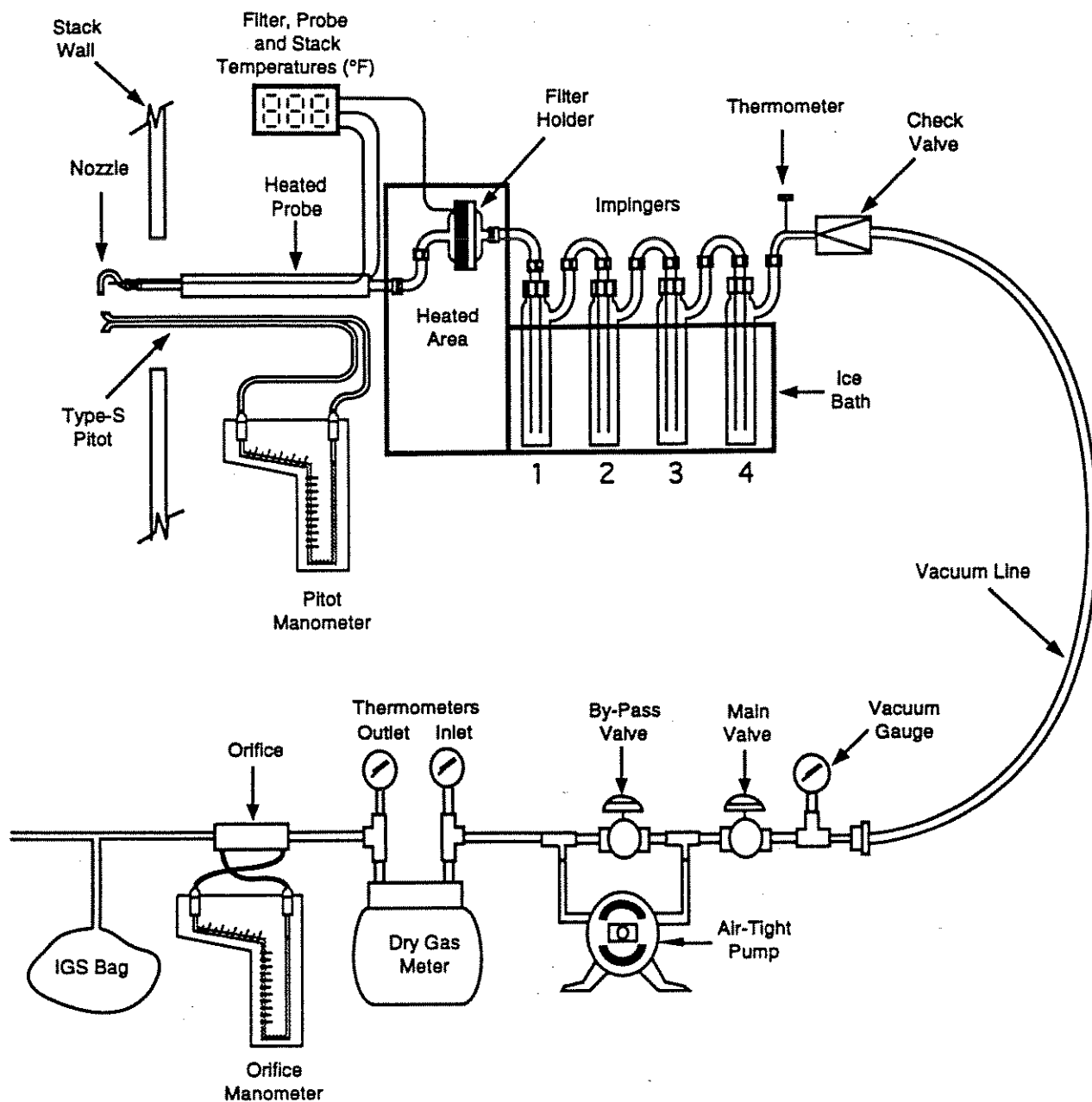
Place a clean, unused filter into a labeled container for a sample blank.

Container 4
Petri Dish

0.1 N HNO₃ Blank

Pour 200 ml of HNO₃ from wash bottle into a labeled container for a sample blank.

Container 5
250 ml Plastic



Method 12- Lead
absorbing solution (0.1 N HNO₃)

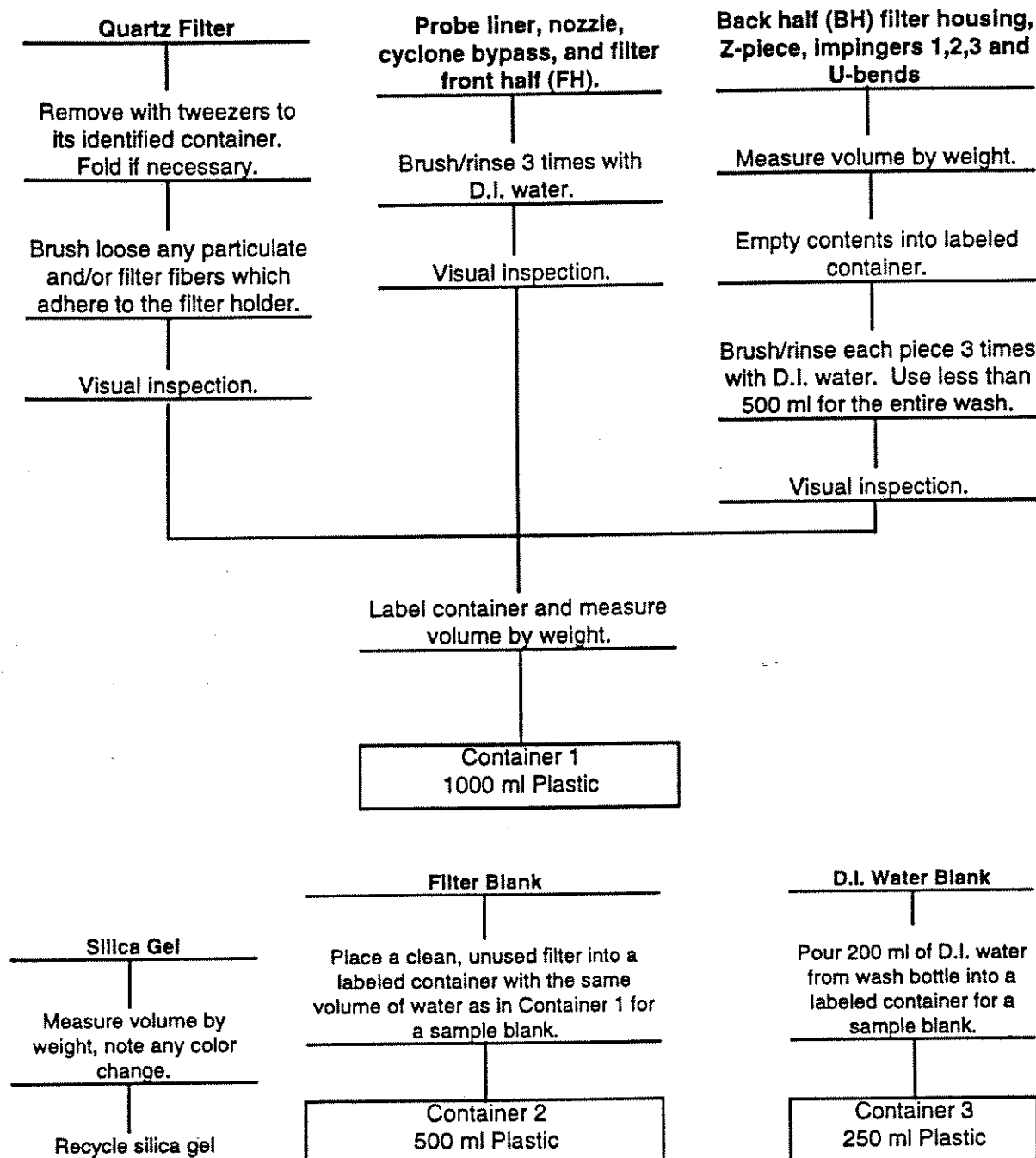
Dilute 6.5 ml of concentrated nitric acid (HNO₃) to 1 liter with DI water

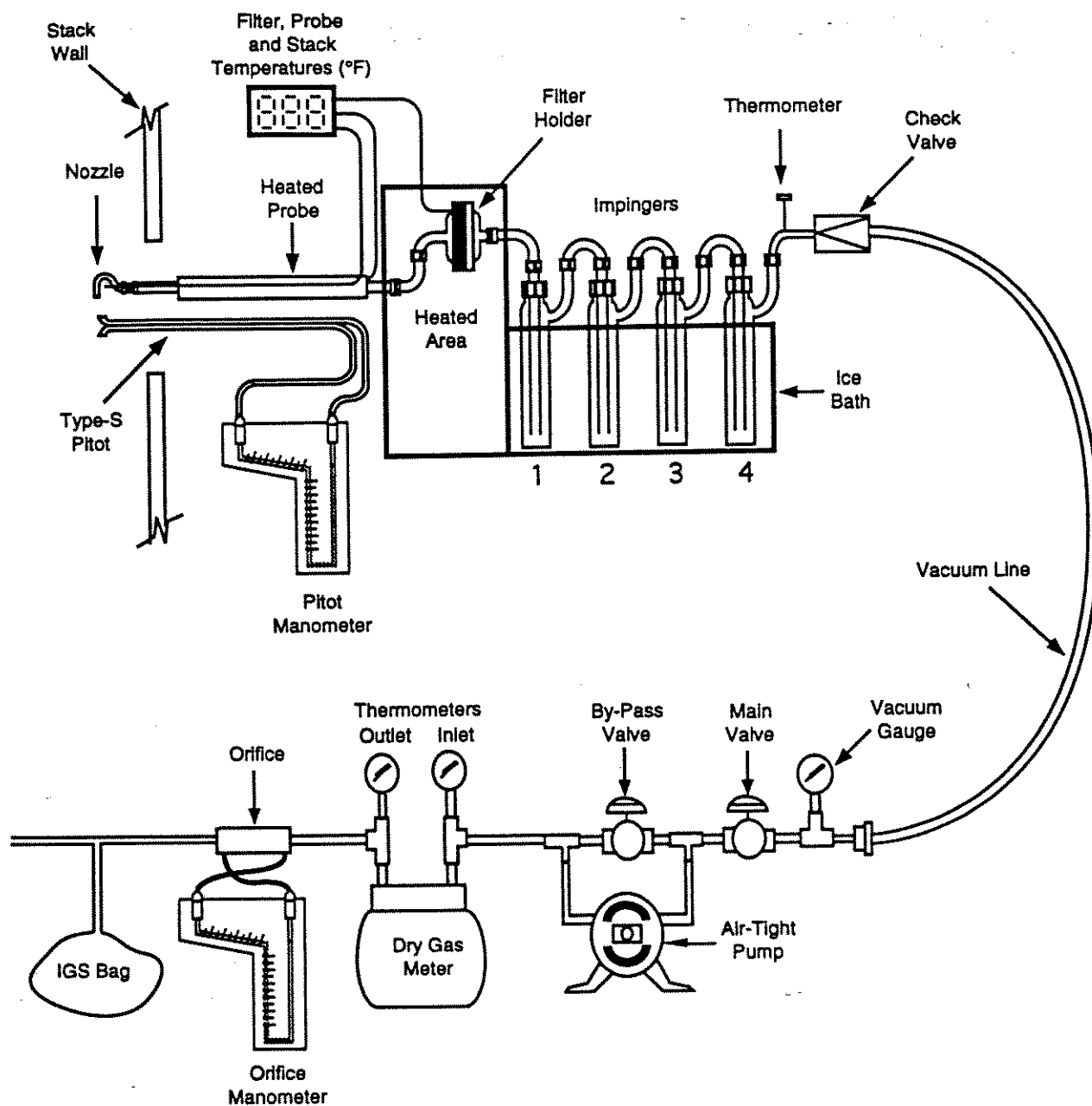
Impinger 1
Impinger 2
Impinger 3
Impinger 4

100 ml 0.1 N HNO₃
100 ml 0.1 N HNO₃
empty
silica gel

METHOD 13B - DETERMINATION OF TOTAL FLUORIDE EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





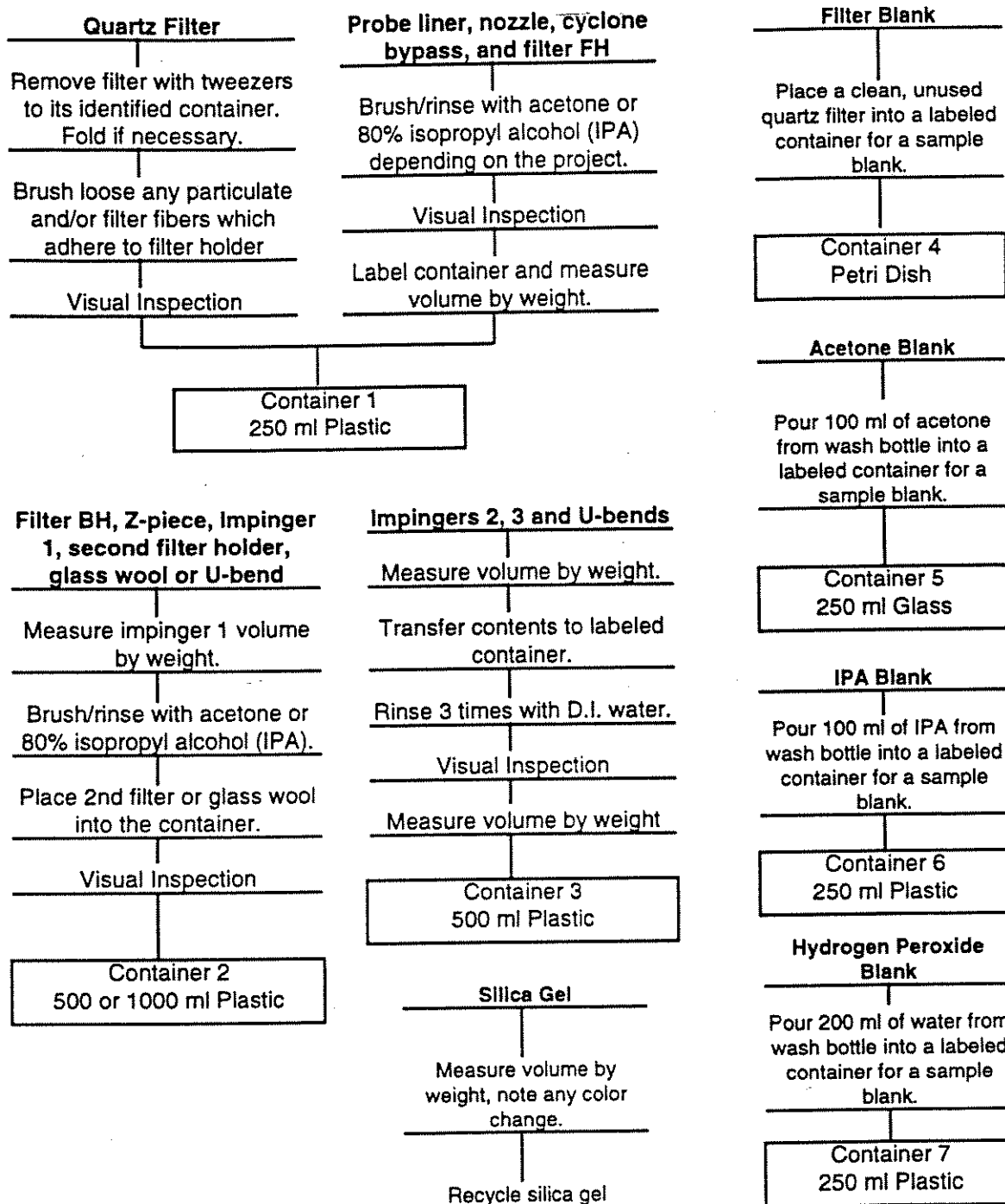
M13B - Hydrogen Fluoride

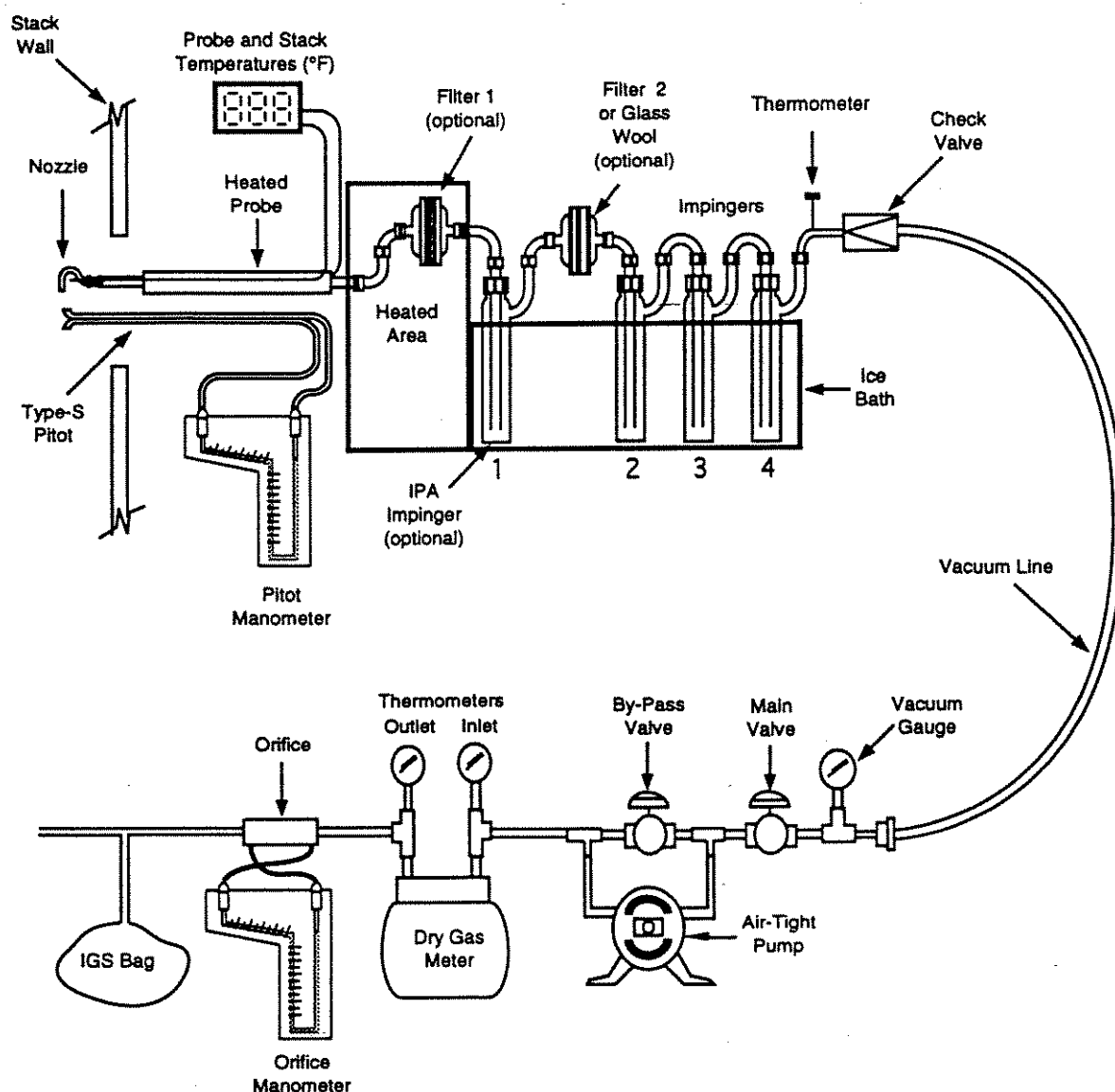
Impinger 1
Impinger 2
Impinger 3
Impinger 4

100 ml DI water
100 ml DI water
empty
silica gel

**METHOD 8 - DETERMINATION OF SULFURIC ACID MIST AND SULFUR DIOXIDE EMISSIONS
FROM STATIONARY SOURCES**

- **Immediately after sampling the train should be purged with ambient air for 15 minutes, during this time the ice bath should also be drained.**
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M8 - Sulfuric Acid Mist and Sulfur Dioxide
absorbing solution (80% IPA)

absorbing solution (3% H_2O_2)

Mix 800 ml isopropanol (IPA) with
200 ml DI water
Dilute 100 ml of 30% hydrogen peroxide (H_2O_2)
with 1 liter of DI water, prepare daily

Impinger 1	100 ml 80% IPA
Impinger 2	100 ml 3% H_2O_2
Impinger 3	100 ml 3% H_2O_2
Impinger 4	silica gel

Filter 1 used only if separating condensed acid mist particles.

Filter 2 or glass wool and IPA Impinger only used when looking for gaseous SO_3 .

METHOD 26 : DETERMINATION OF HYDROGEN CHLORIDE EMISSIONS FROM
STATIONARY SOURCES

(NO SODIUM HYDROXIDE IMPINGER)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Teflon Filter

No recovery necessary

Impingers 1,2,3 and U-bends

Empty contents into container.

Rinse components 3x with D.I. water

Label container and measure volume by weight.

Visual inspection

Container 1
500 ml plastic

Sulfuric Acid
Blank(H_2SO_4)

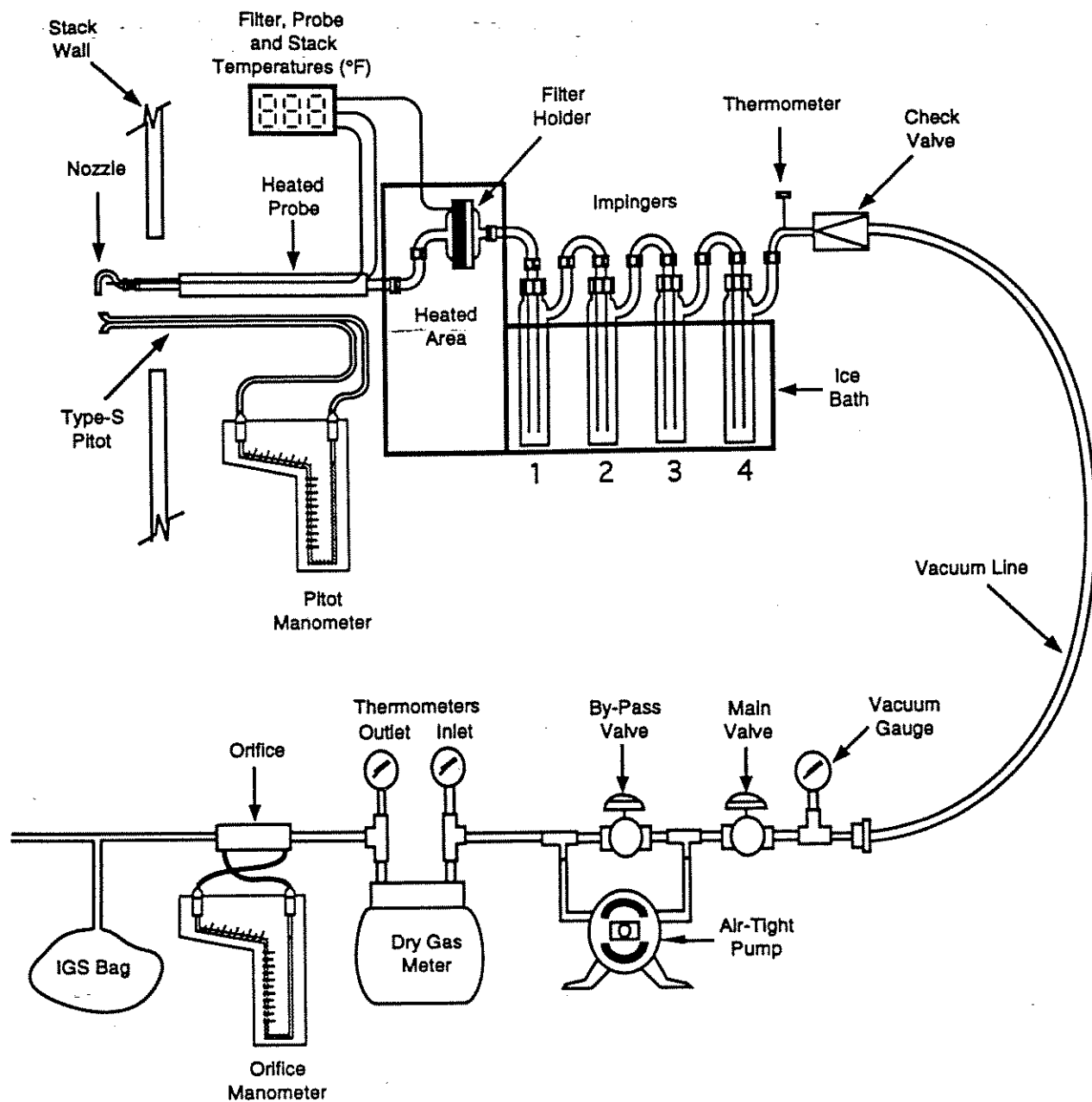
Pour 200 ml of 0.1N H_2SO_4
in a labeled container for a
sample blank.

Container 2
250 ml plastic

Silica Gel

Measure volume by
weight, note any color
change.

Recycle silica gel



Modified M26 - Hydrogen Chloride
absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

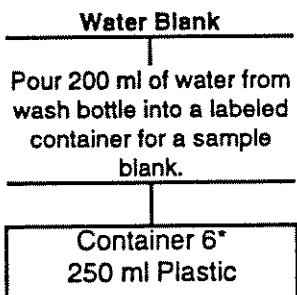
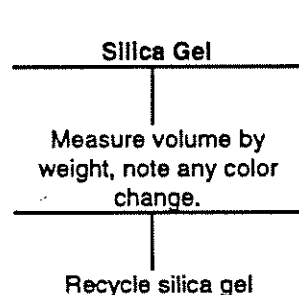
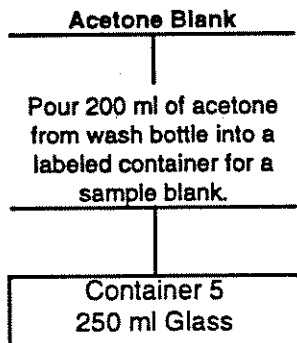
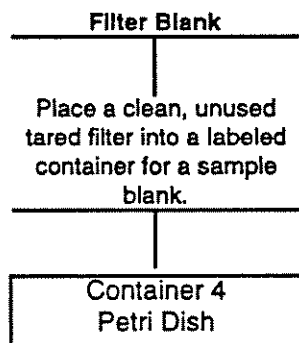
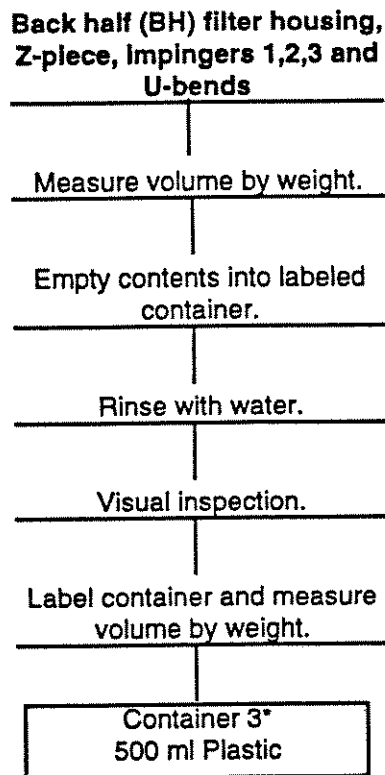
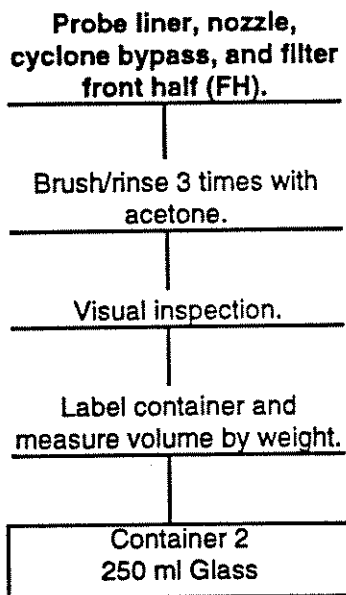
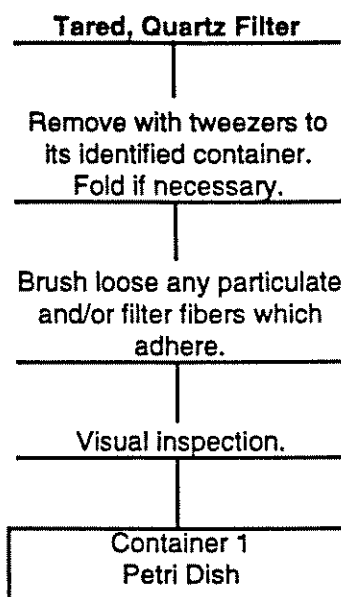
Impinger 1
Impinger 2
Impinger 3
Impinger 4

100 ml 0.1 N H_2SO_4
100 ml 0.1 N H_2SO_4
empty
silica gel

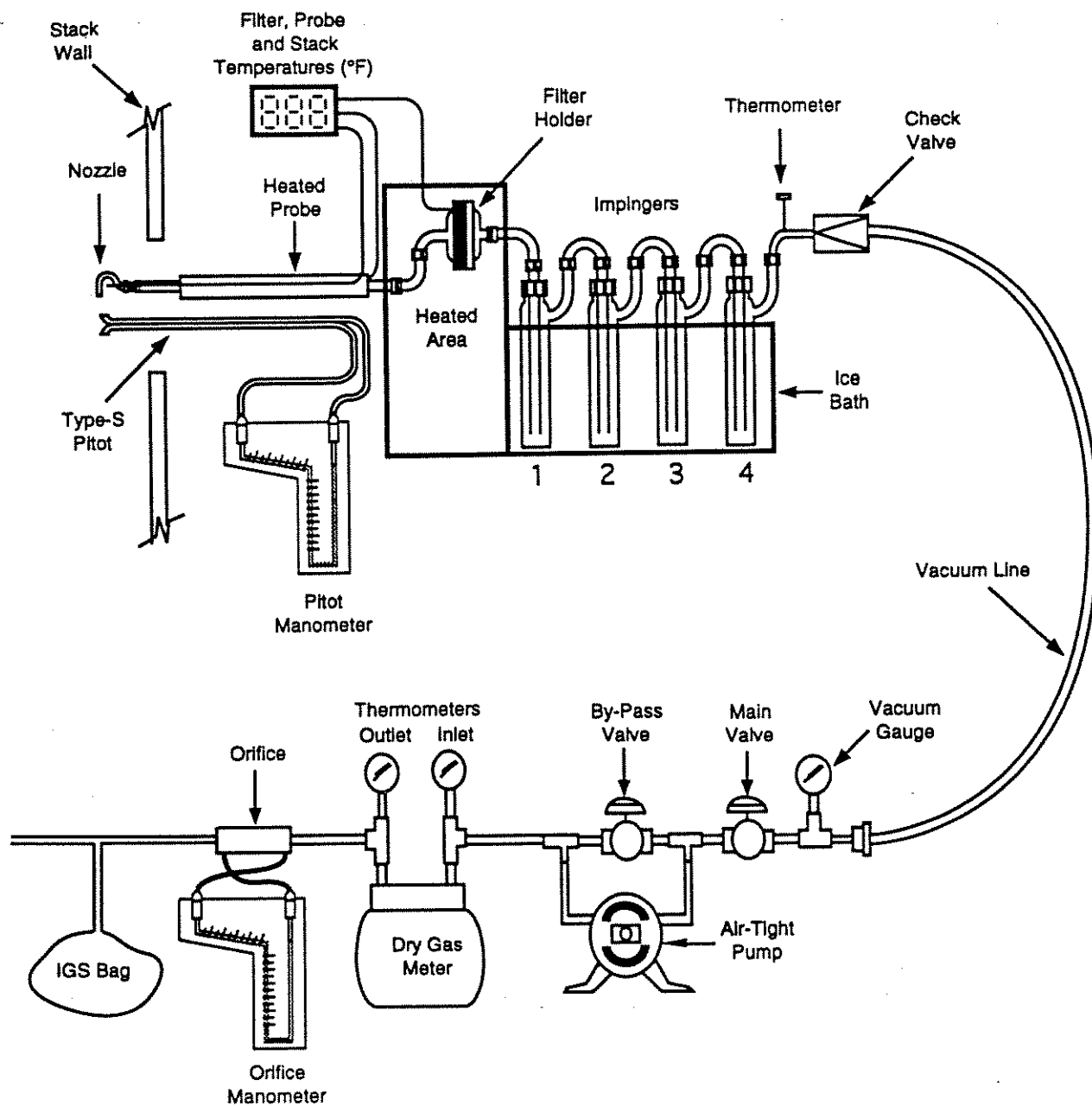
Note: This is generally single point non-isokinetic sampling train.

METHOD 5 - DETERMINATION OF PARTICULATE EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).



*Containers 3 and 6 are required only when the testing includes a back half analysis.



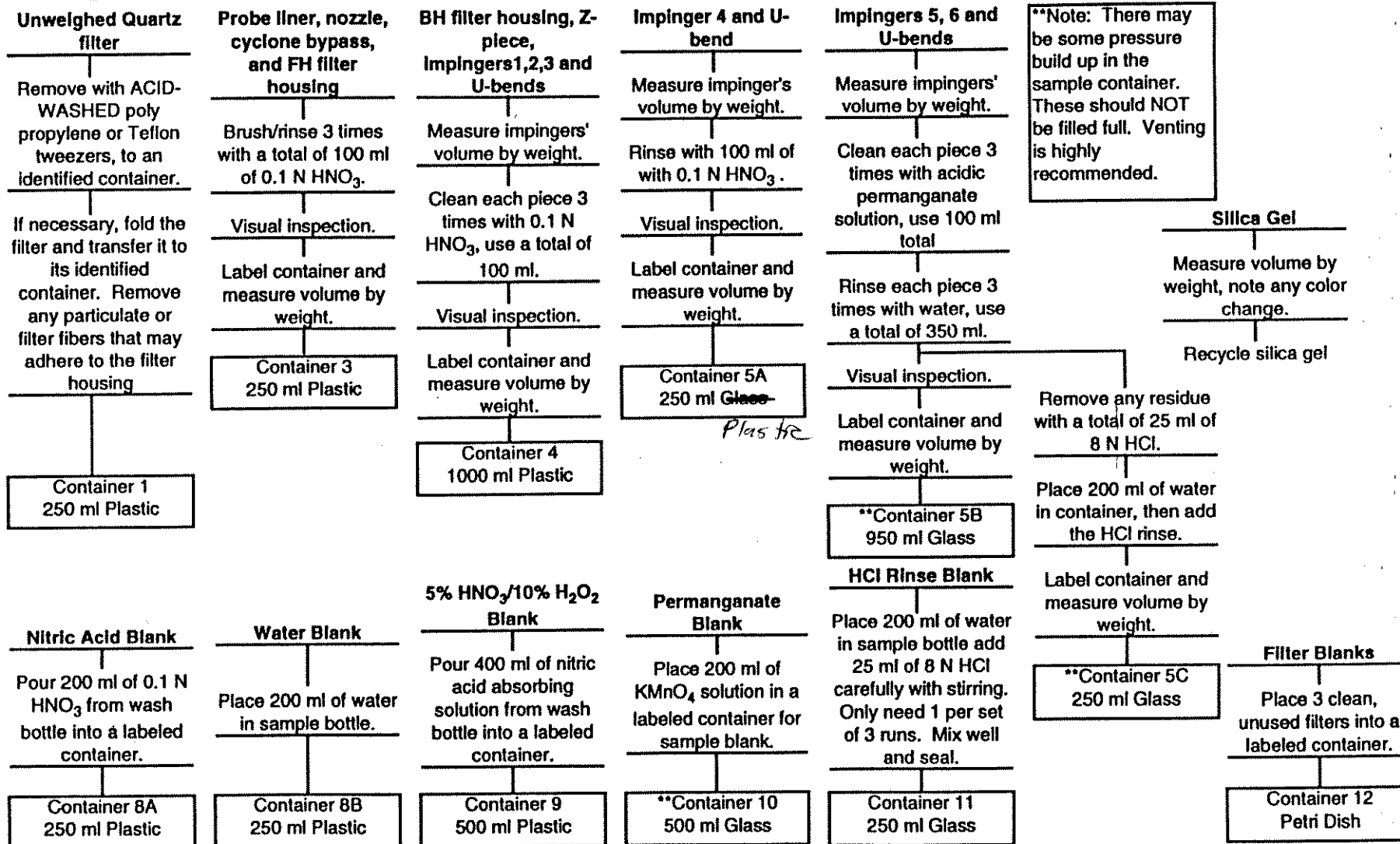
M5 - Particulate

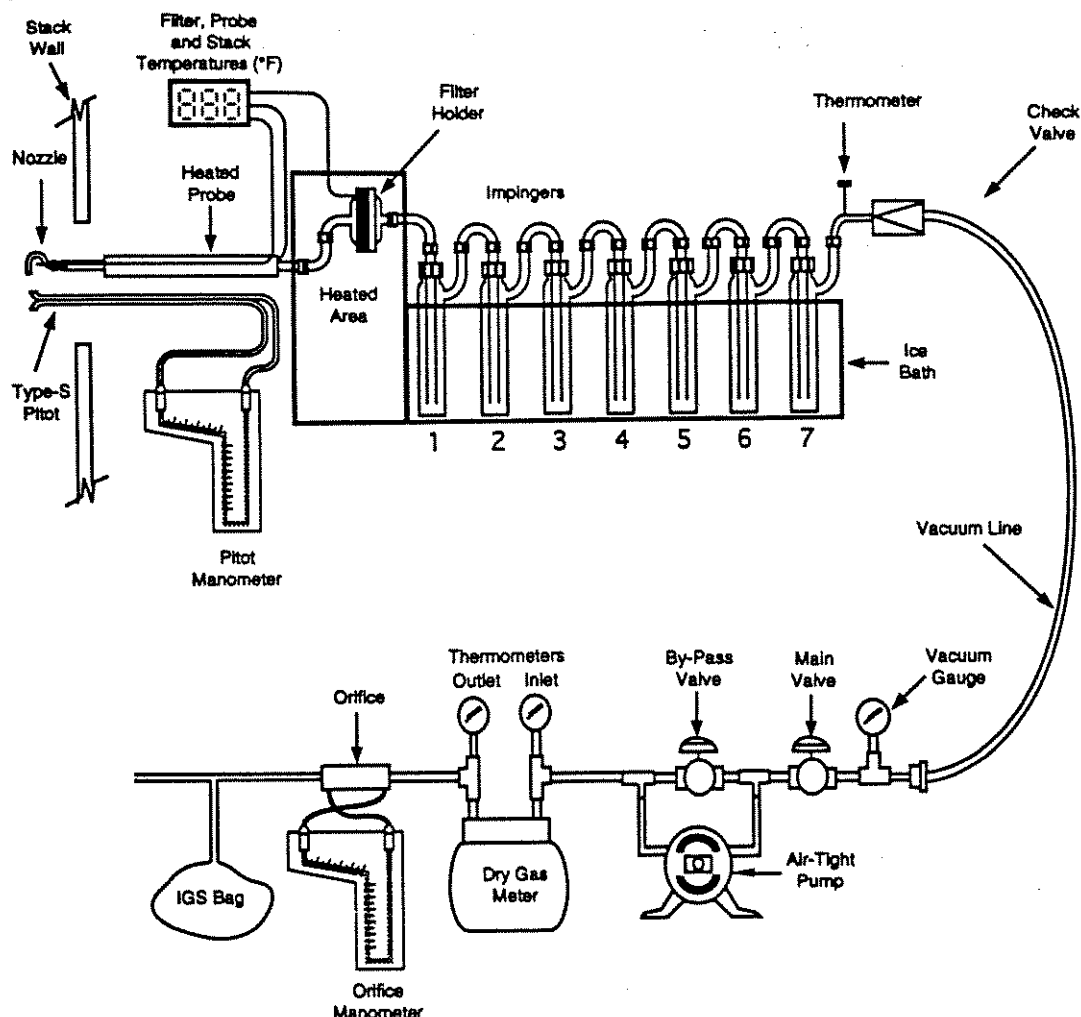
Impinger 1	100 ml H ₂ O
Impinger 2	100 ml H ₂ O
Impinger 3	empty
Impinger 4	silica gel

METHOD 29 - DETERMINATION OF METALS EMISSIONS FROM STATIONARY SOURCES

(INCLUDING MERCURY DETERMINATION, EXCLUDING PARTICULATE DETERMINATION)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





Proposed EPA Method 29 - Metals

Metals absorbing soln (5% HNO_3 /10% H_2O_2)

Mix 50 ml concentrated nitric acid (HNO_3) in 500 ml of DIUF water, add 333 ml of 30% H_2O_2 and dilute to 1 liter

Mercury absorbing solution (4% KMnO_4 /10% H_2SO_4)

Dissolve, with stirring, 40 grams potassium permanganate (KMnO_4) in 900 ml of DIUF water. Slowly add 100 ml concentrated sulfuric acid (H_2SO_4) and mix well, just prior to testing.

Mercury rinse solution (8N HCl)

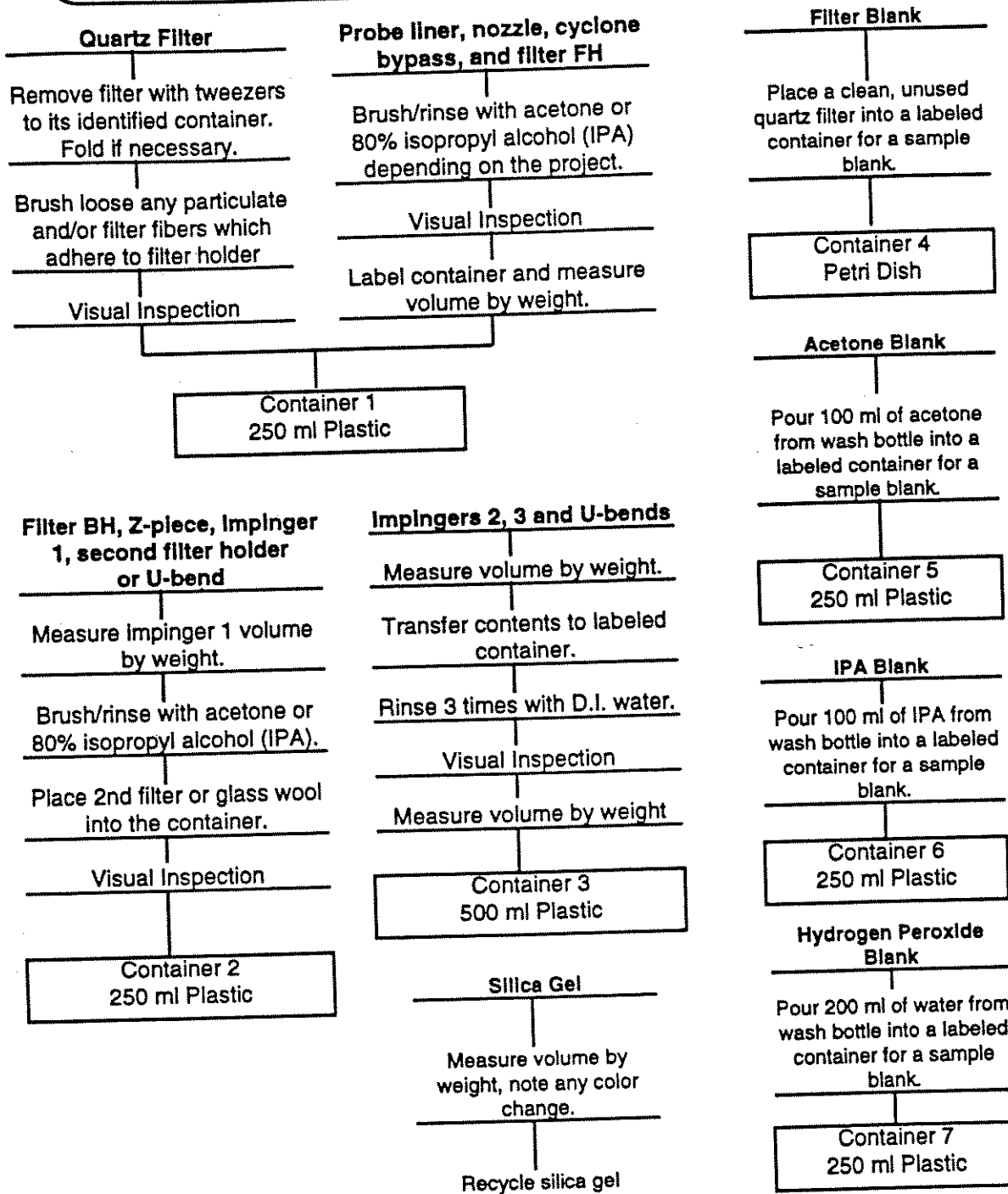
Add 69 ml of concentrated HCl to 25 ml deionized distilled water (Add acid to water). Dilute with DIUF water to 100 ml.

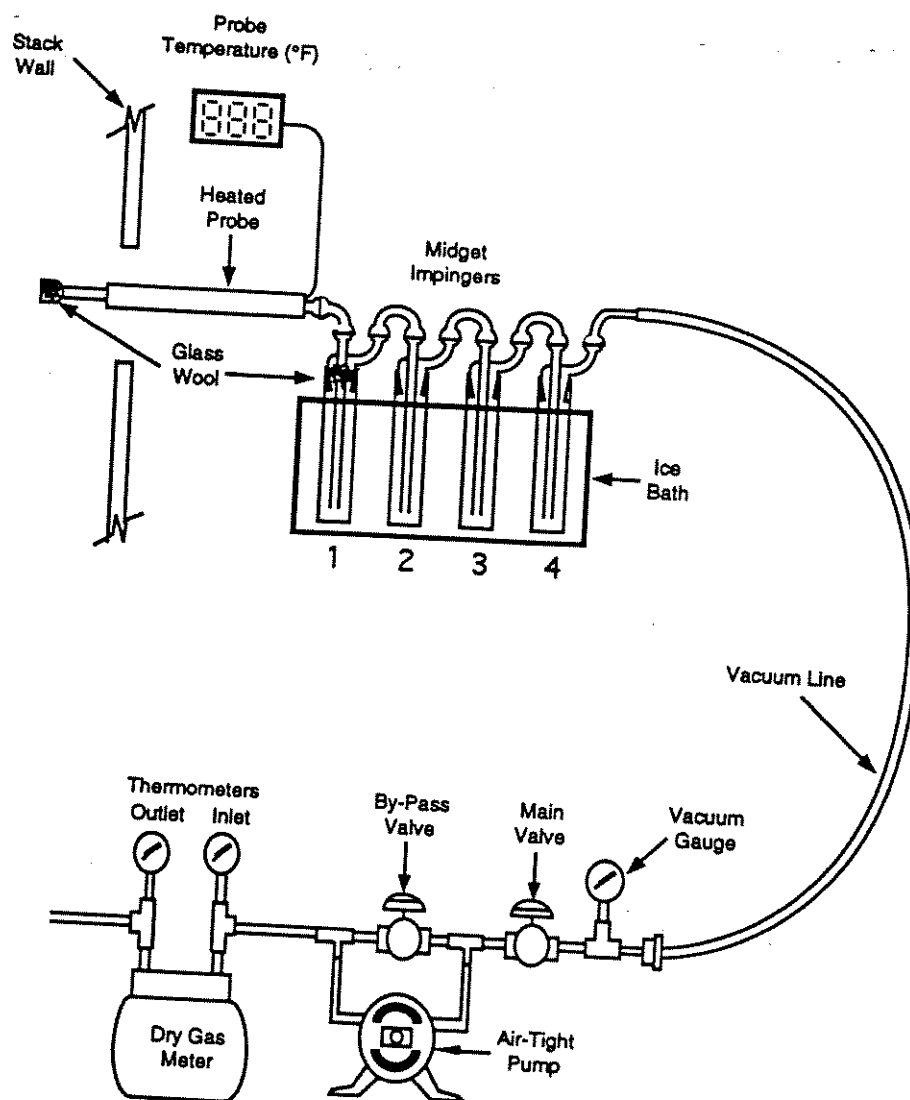
Impinger 1	empty
Impinger 2	100 ml 5% HNO_3 /10% H_2O_2
Impinger 3	100 ml 5% HNO_3 /10% H_2O_2
Impinger 4	empty
Impinger 5	100 ml 4% KMnO_4 /10% H_2SO_4
Impinger 6	100 ml 4% KMnO_4 /10% H_2SO_4
Impinger 7	silica gel

Note: If mercury emissions are not to be determined, then the mercury absorbing solution and mercury rinse solution as well as Impingers 5 and 6 are not needed.

METHOD 6 - DETERMINATION OF SULFUR DIOXIDE EMISSIONS FROM STATIONARY SOURCES

- Immediately after sampling the train should be purged with ambient air for 15 minutes, during this time the ice bath should also be drained.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M6 - Sulfur Dioxide
absorbing solution (80% IPA)

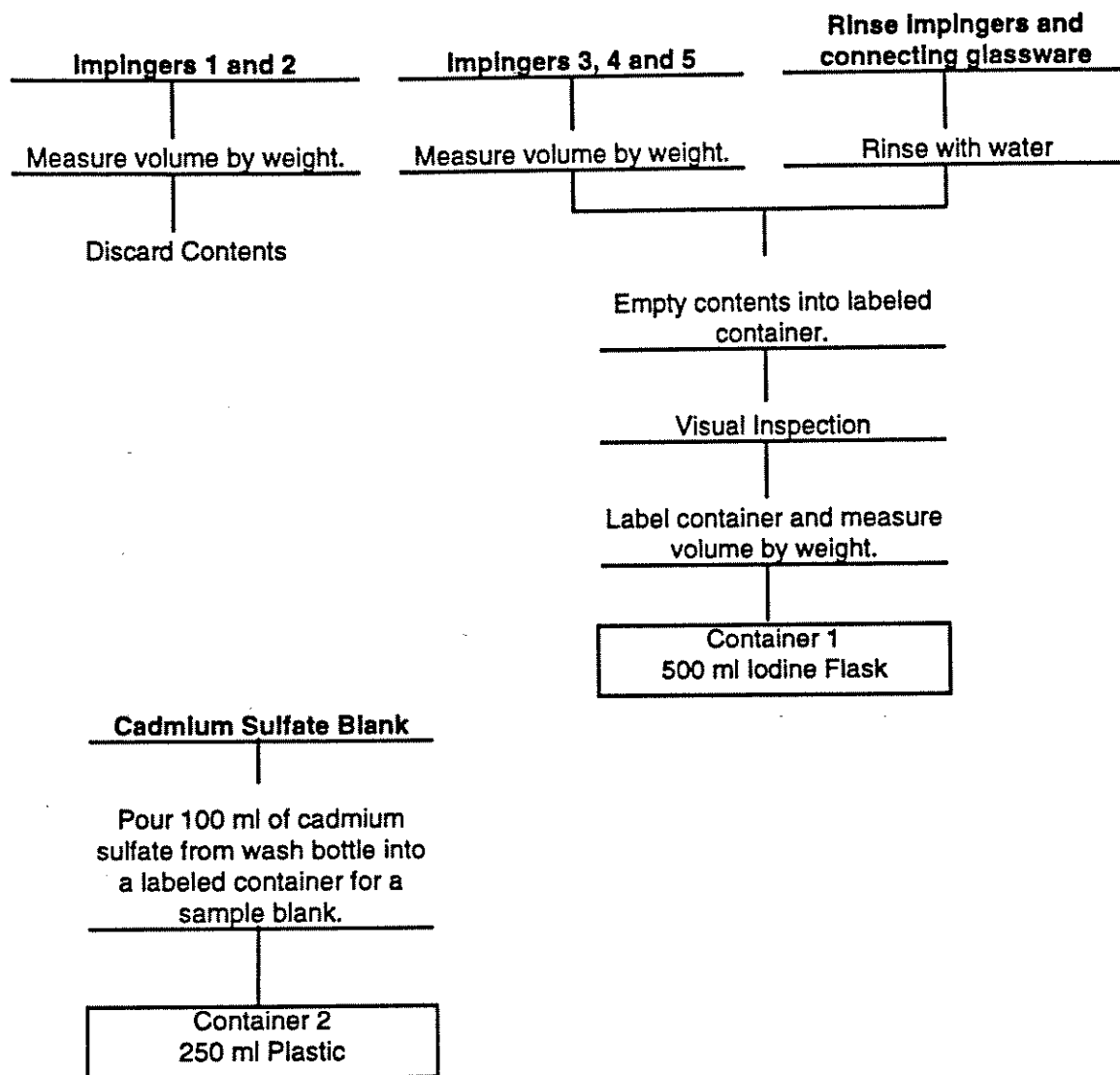
absorbing solution (3% H_2O_2)

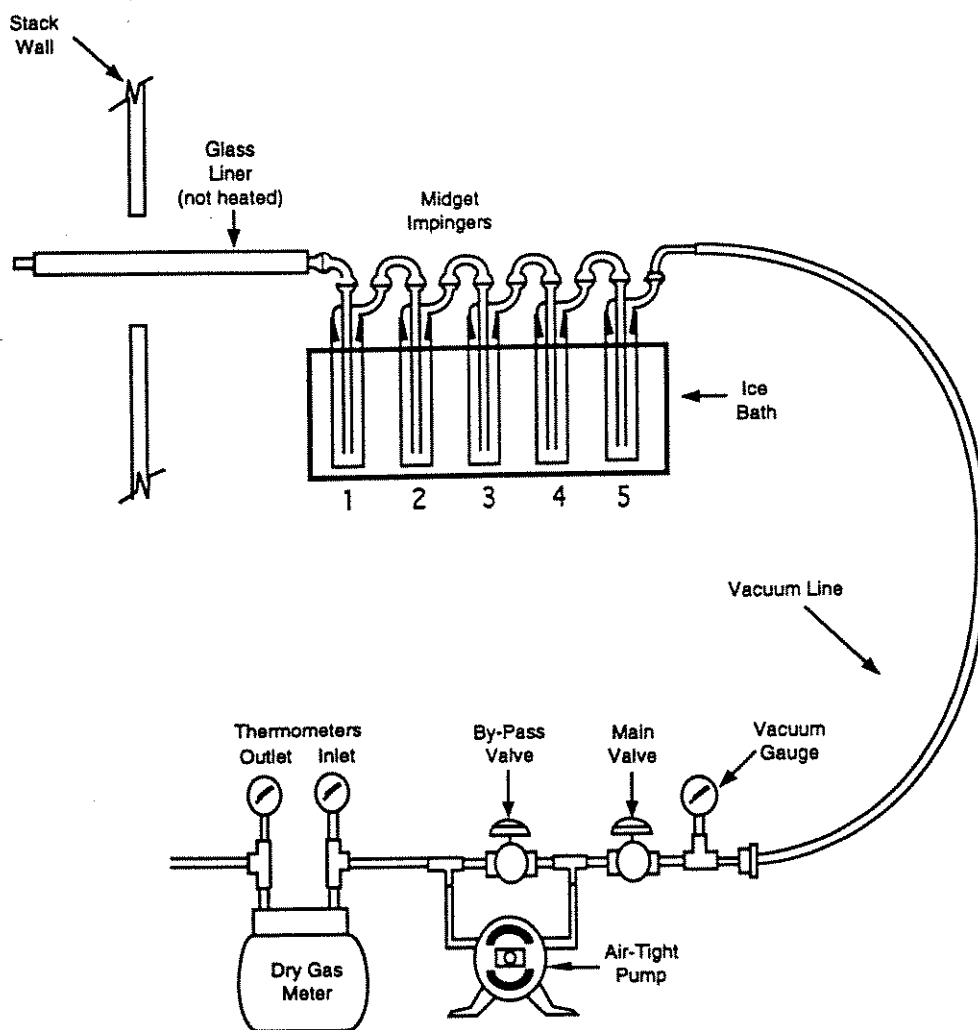
Midget Bubbler
Midget Impinger 1
Midget Impinger 2
Midget Impinger 3

Mix 800 ml isopropanol (IPA) with
200 ml DI water
Dilute 100 ml of 30% Hydrogen peroxide (H_2O_2)
with 1 liter of DI water, prepare daily
15 ml 80% IPA
15 ml 3% H_2O_2
15 ml 3% H_2O_2
empty

METHOD 11 - DETERMINATION OF HYDROGEN SULFIDE CONTENT OF FUEL GAS
STREAMS IN PETROLEUM REFINERIES

- Immediately after sampling the train should be purged with ambient air for 15 minutes, during this time the ice bath should also be drained.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.





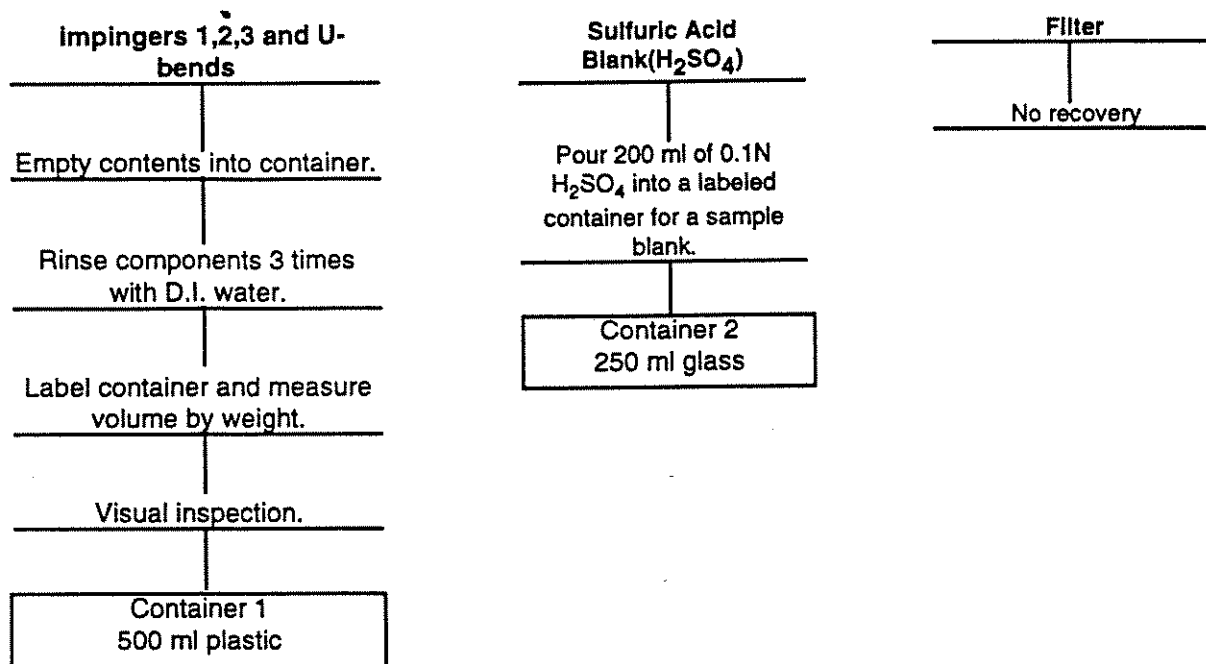
Method 11 - Hydrogen Sulfide
 absorbing solution (3% H_2O_2)
 absorbing solution (cadmium sulfate)

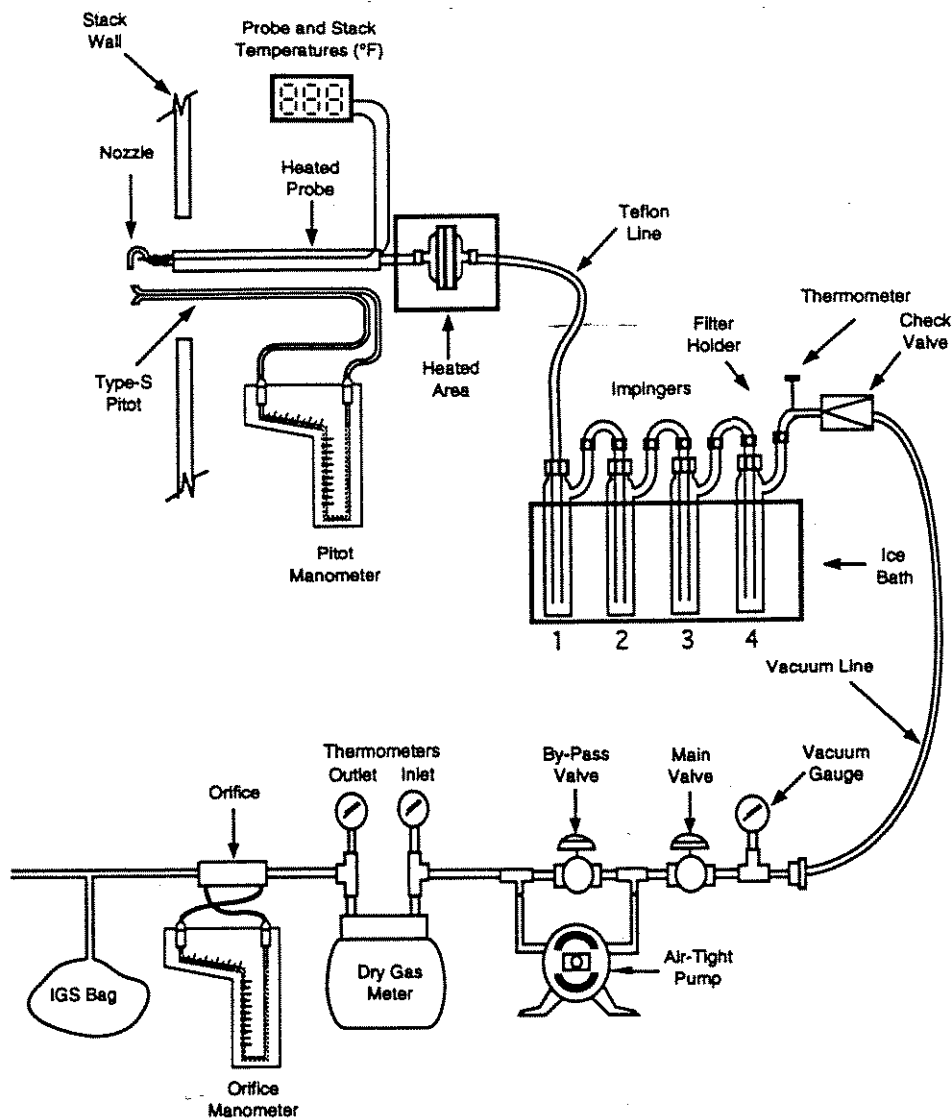
Dilute 100 ml of 30% Hydrogen peroxide (H_2O_2)
 with 1 liter of DI water
 Dissolve 41 g of $3\text{CdSO}_4 \cdot 8\text{H}_2\text{O}$ and 15 ml of 0.1 M
 sulfuric acid in a 1-liter volumetric flask that contains
 approximately 3/4 liter of DI water

Midget Impinger 1	15 ml 3% hydrogen peroxide
Midget Impinger 2	empty
Midget Impinger 3	15 ml cadmium sulfate
Midget Impinger 4	15 ml cadmium sulfate
Midget Impinger 5	15 ml cadmium sulfate

METHOD 13B/26: - DETERMINATION OF FLUORIDE/HYDROGEN CHLORIDE EMISSIONS
FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





Modified M26 - Hydrogen Chloride
absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

Impinger 1	100 ml 0.1 N H_2SO_4
Impinger 2	100 ml 0.1 N H_2SO_4
Impinger 3	empty
Impinger 4	silica gel

Note: This is generally single point non-isokinetic sampling train.

METHOD 16A - DETERMINATION OF TOTAL REDUCED SULFUR EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

**Midget Impingers from the
Method 6 part of the train
and connecting tubing**

Pour impinger contents into a
polyethylene sample
container.

Rinse all components with
water.

Visual Inspection

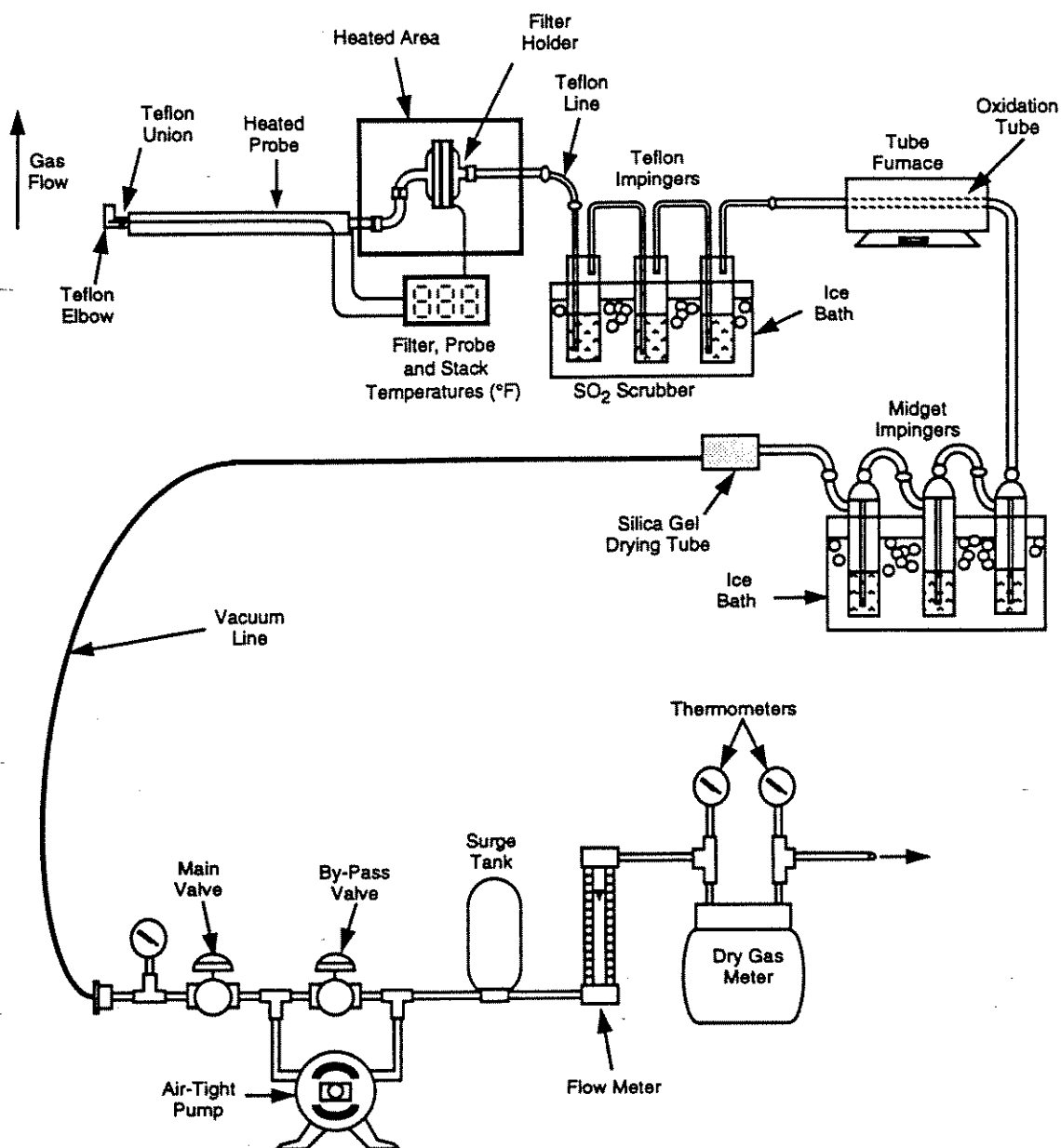
Label container and measure
volume by weight.

Container 1
125 ml Plastic

Silica Gel

Measure volume by
weight, note any color
change.

Recycle silica gel



**M16A - Total Reduced Sulfur
Citrate Buffer**

absorbing solution (3% H_2O_2)

SO_2 Scrubber

Impinger 1
Impinger 2
Impinger 3

Method 6 Part of Train

Midget Impinger 1
Midget Impinger 2
Midget Impinger 3

300 g of potassium citrate and 41 g of anhydrous citric acid dissolved in 1 liter of water. Adjust pH (5.4-5.6) with potassium citrate or citric acid as needed.

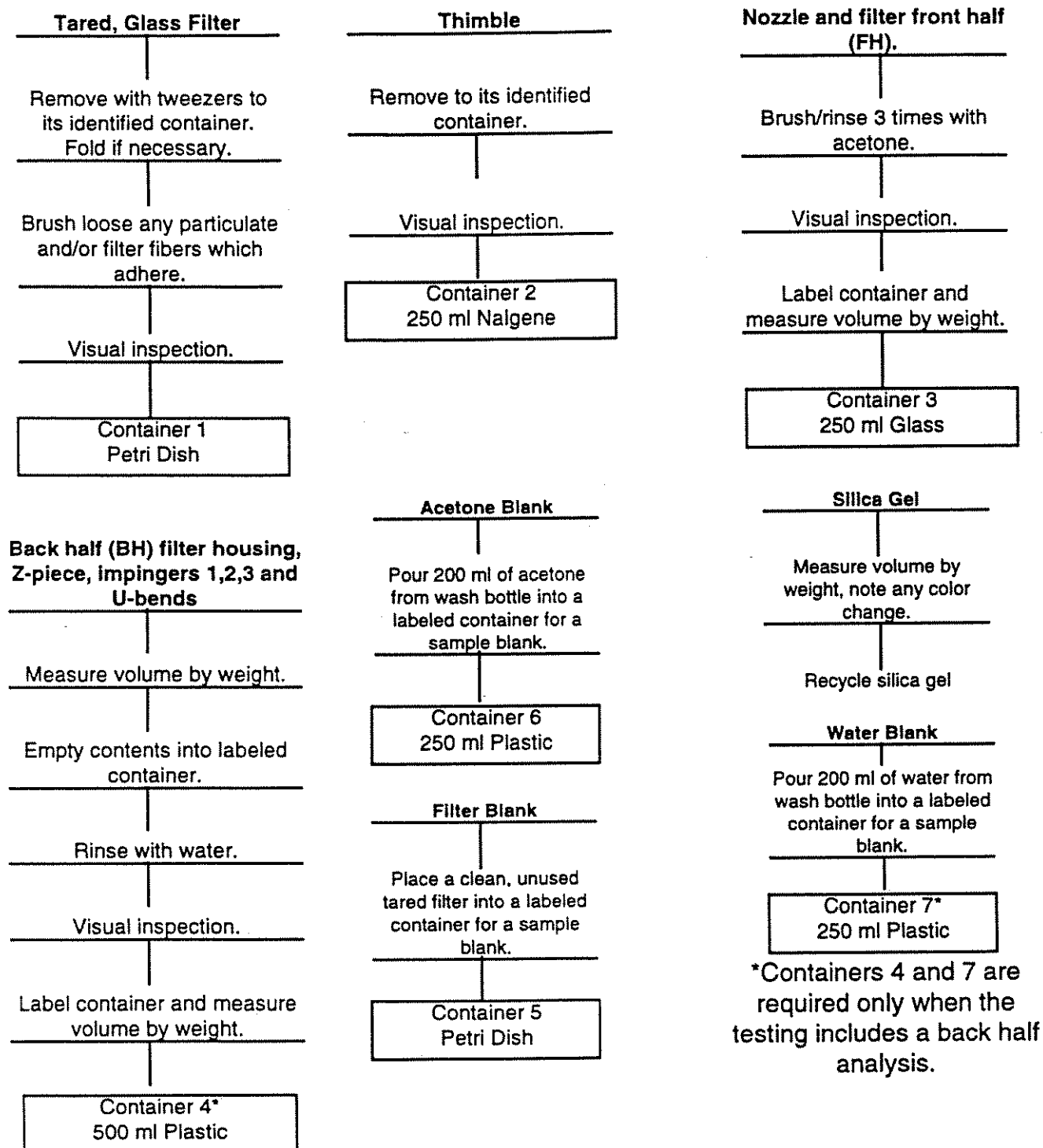
Dilute 100 ml of 30% Hydrogen peroxide (H_2O_2) with 1 liter of DI water, prepare daily

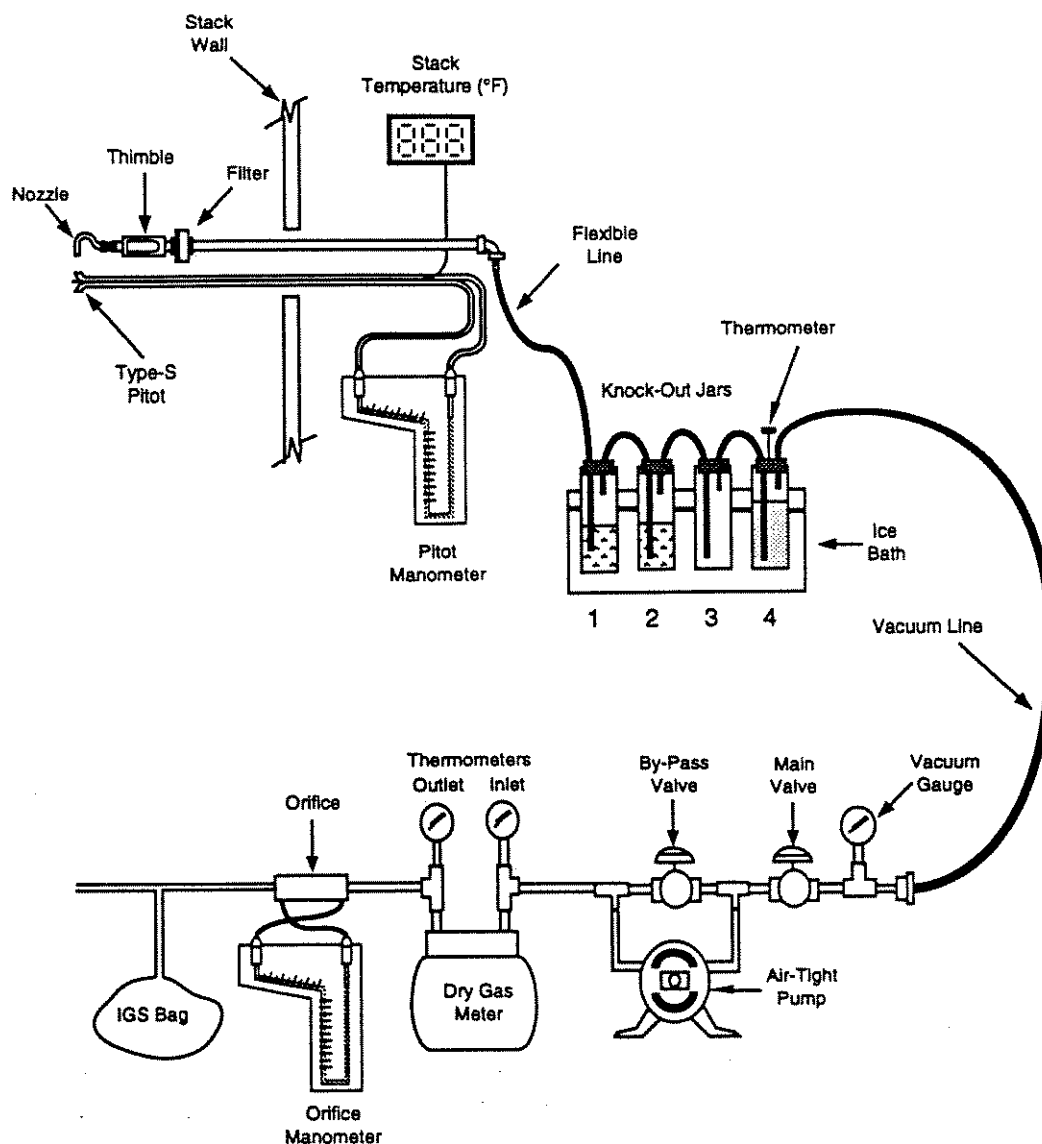
100 ml citrate buffer
100 ml citrate buffer
empty

20 ml 3% H_2O_2
20 ml 3% H_2O_2
empty

METHOD 17 - DETERMINATION OF PARTICULATE EMISSIONS FROM STATIONARY SOURCES (IN-STACK FILTRATION METHOD)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M17 - Particulate

Knock-out Jar 1	100 ml H ₂ O
Knock-out Jar 2	100 ml H ₂ O
Knock-out Jar 3	empty
Knock-out Jar 4	silica gel

METHOD 0011- DETERMINATION OF FORMALDEHYDE EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Probe liner, nozzle, cyclone
bypass, and filter filter
bypass.

Brush/rinse 3 times with MeCl.

Visual inspection.

Impingers 1,2,3 and U-bends

Measure volume by weight.

Empty contents into labeled
Container 1.

Brush/rinse each piece 3 times
with MeCl. Rinse 3X with
HPLC water. All into
Container 1

Visual inspection.

Label container and
measure volume by weight.

Container 1
1000 ml Glass

Silica Gel

Measure volume by
weight, note any color
change.

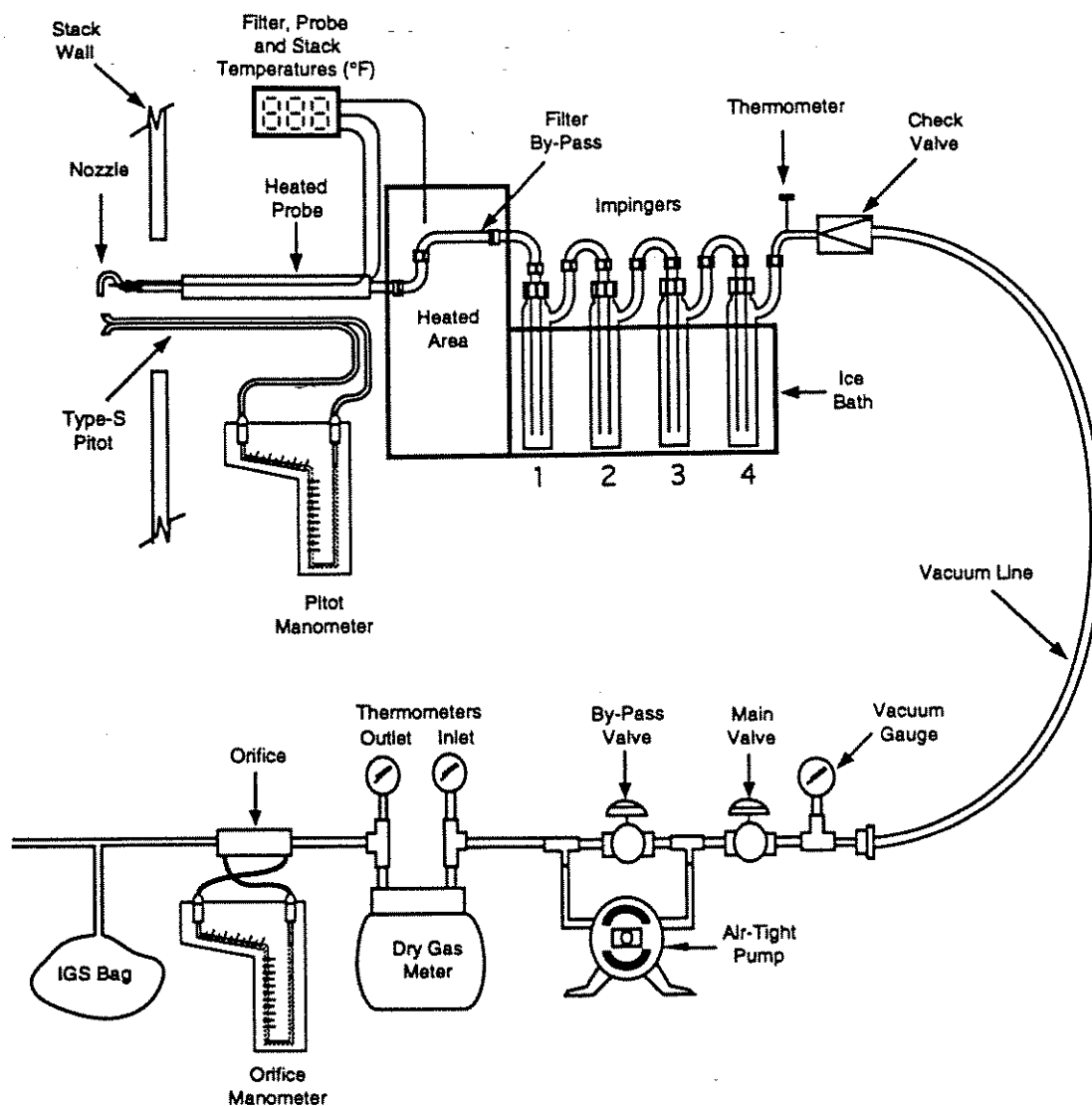
Recycle silica gel

DNPH Blank

Pour DNPH and MeCl into
a labeled container to the
approximate total volume
of Container 1.

Container 2

Note: Try to use a total of
less than 250 ml of DNPH
to rinse each train.
Definitely use less than
500 ml. Samples should
be kept cool.



**M0011 - Aldehyde and Ketone
absorbing solution (DNPH)**

2,4-dinitrophenylhydrazine; Obtain from laboratory
doing the analysis. This solution can be very
dangerous. Once prepared the shelf life is 3 days.

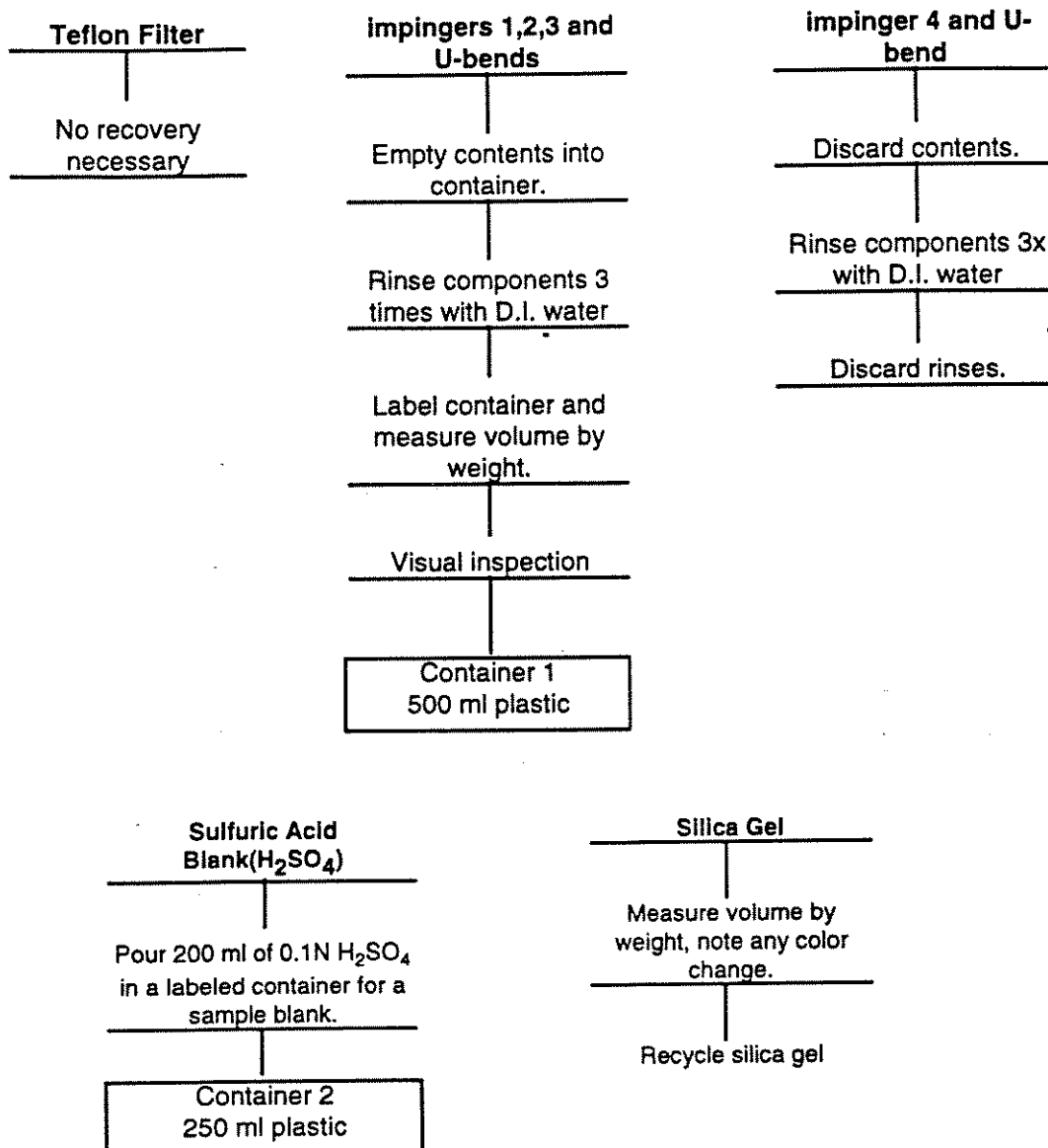
Impinger 1
Impinger 2
Impinger 3
Impinger 4

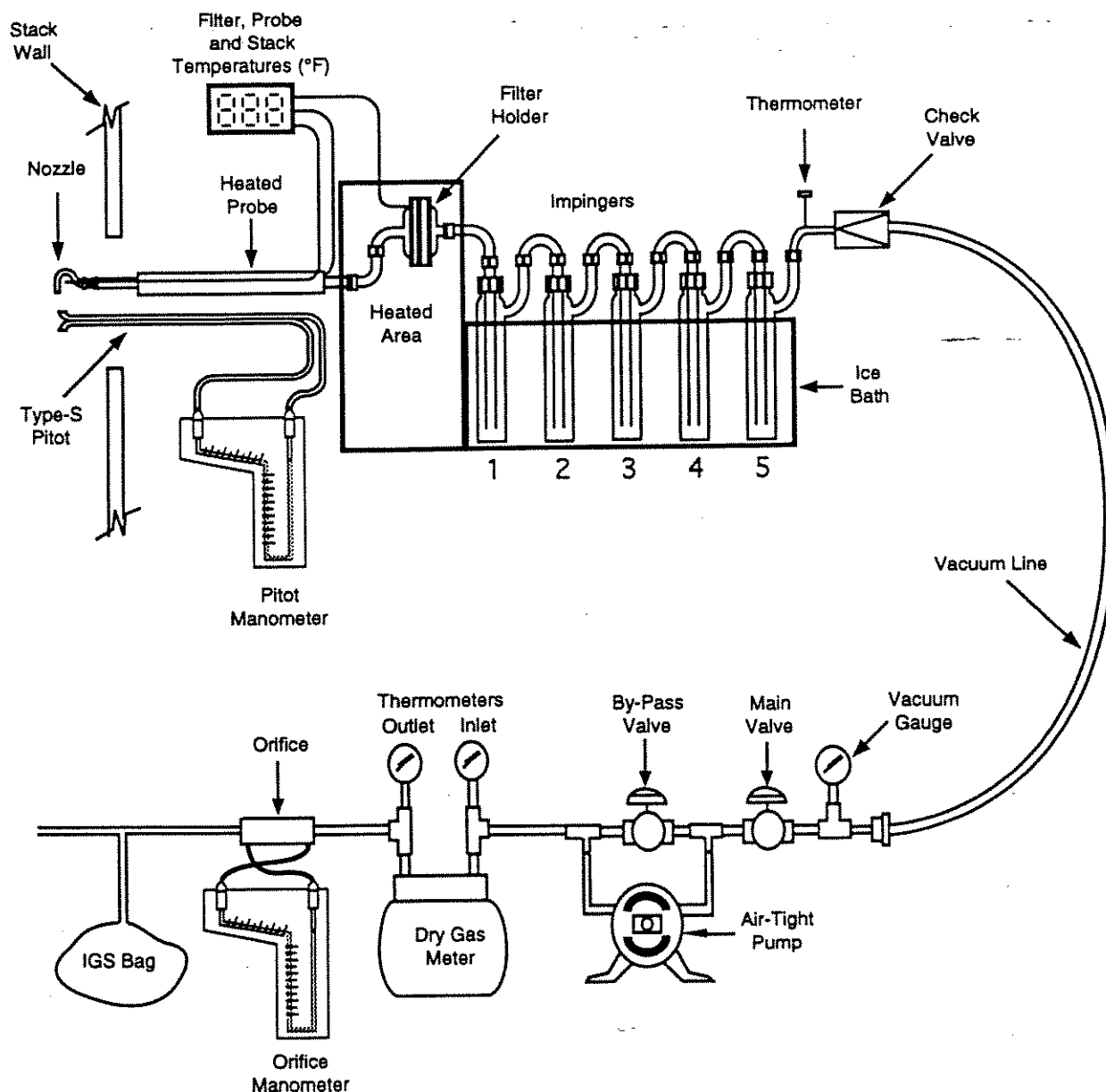
100 ml DNPH
100 ml DNPH
empty
silica gel

METHOD 26 : DETERMINATION OF HYDROGEN CHLORIDE EMISSIONS FROM
STATIONARY SOURCES

(INCLUDING SODIUM HYDROXIDE IMPINGER)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M26 - Hydrogen Chloride
absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

chlorine scrubber solution (0.1 N NaOH)

Dissolve 4.0 grams of solid NaOH in approximately 1000 ml of DI water. Shake well to mix the solution.

Impinger 1
Impinger 2
Impinger 3
Impinger 4
Impinger 5

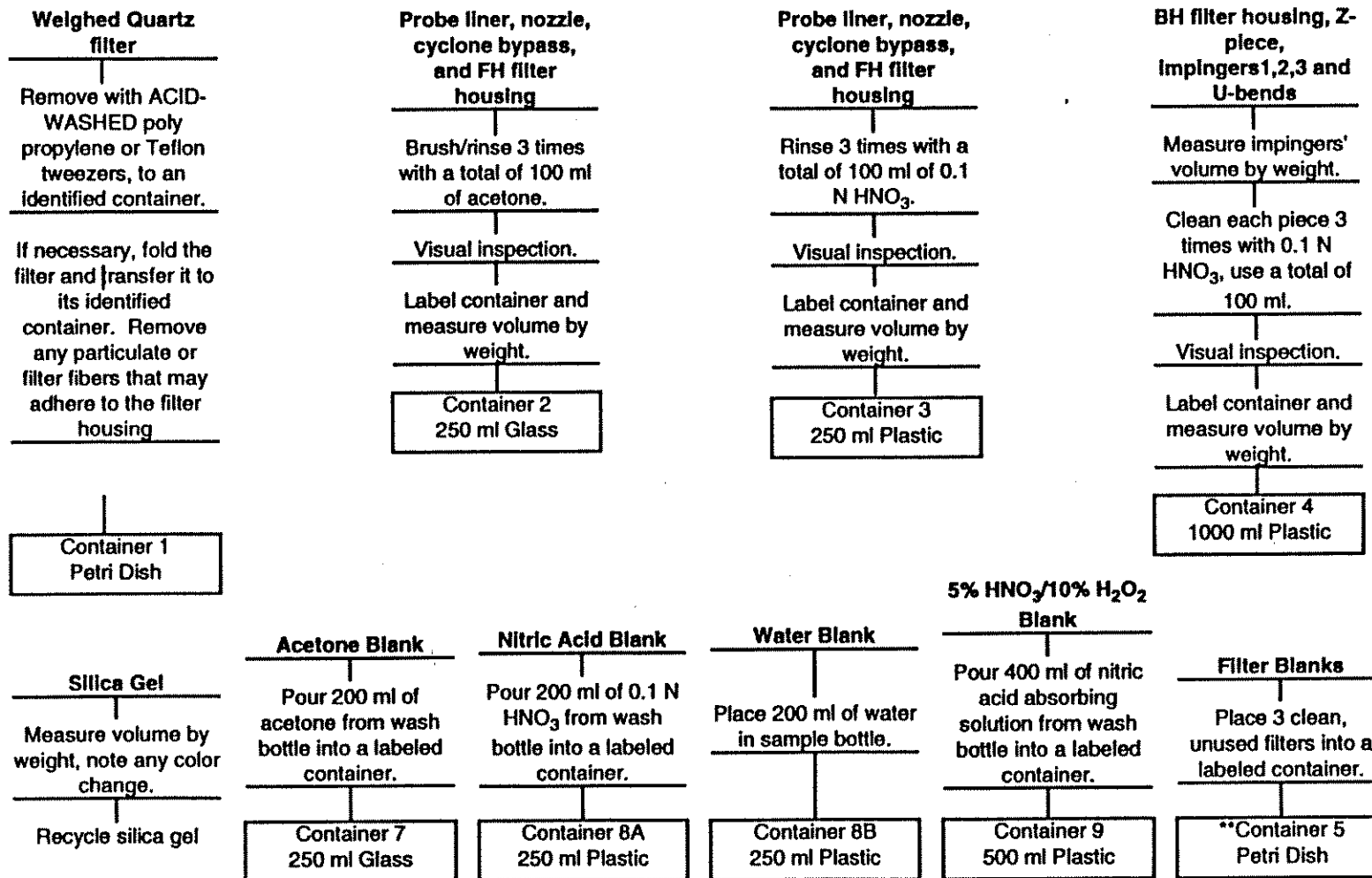
empty
15 ml 0.1 N H_2SO_4
15 ml 0.1 N H_2SO_4
15 ml 0.1 N NaOH
silica gel

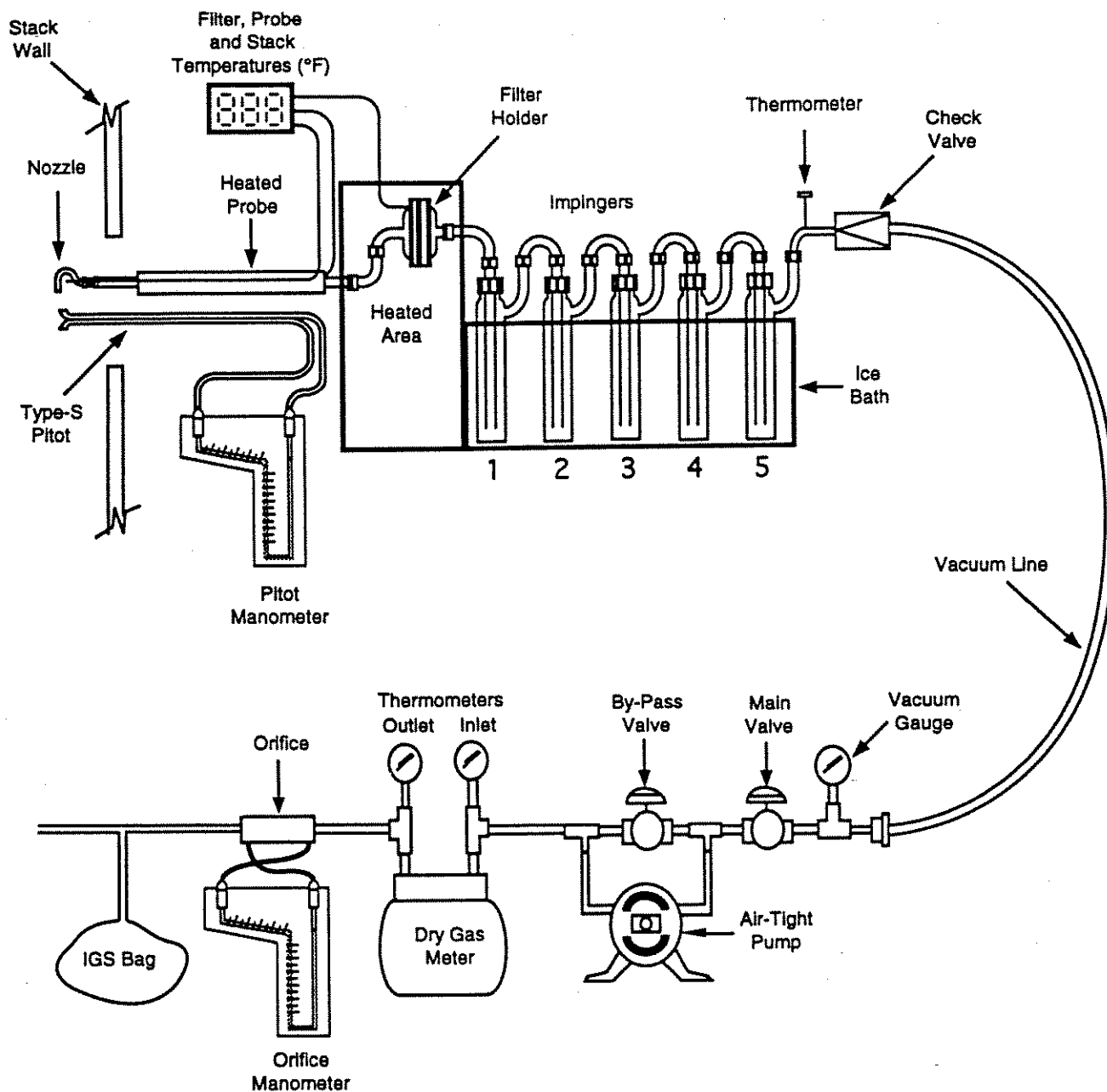
Note: This is a single point non-isokinetic sampling train.

METHOD 29 - DETERMINATION OF METALS EMISSIONS FROM STATIONARY SOURCES

(INCLUDING PARTICULATE DETERMINATION, EXCLUDING MERCURY DETERMINATION)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





~~Proposed~~ EPA Method 29 - Metals

Metals absorbing soln (5% HNO_3 /10% H_2O_2)

Mix 50 ml concentrated nitric acid (HNO_3) in 500 ml of DIUF water, add 333 ml of 30% H_2O_2 and dilute to 1 liter

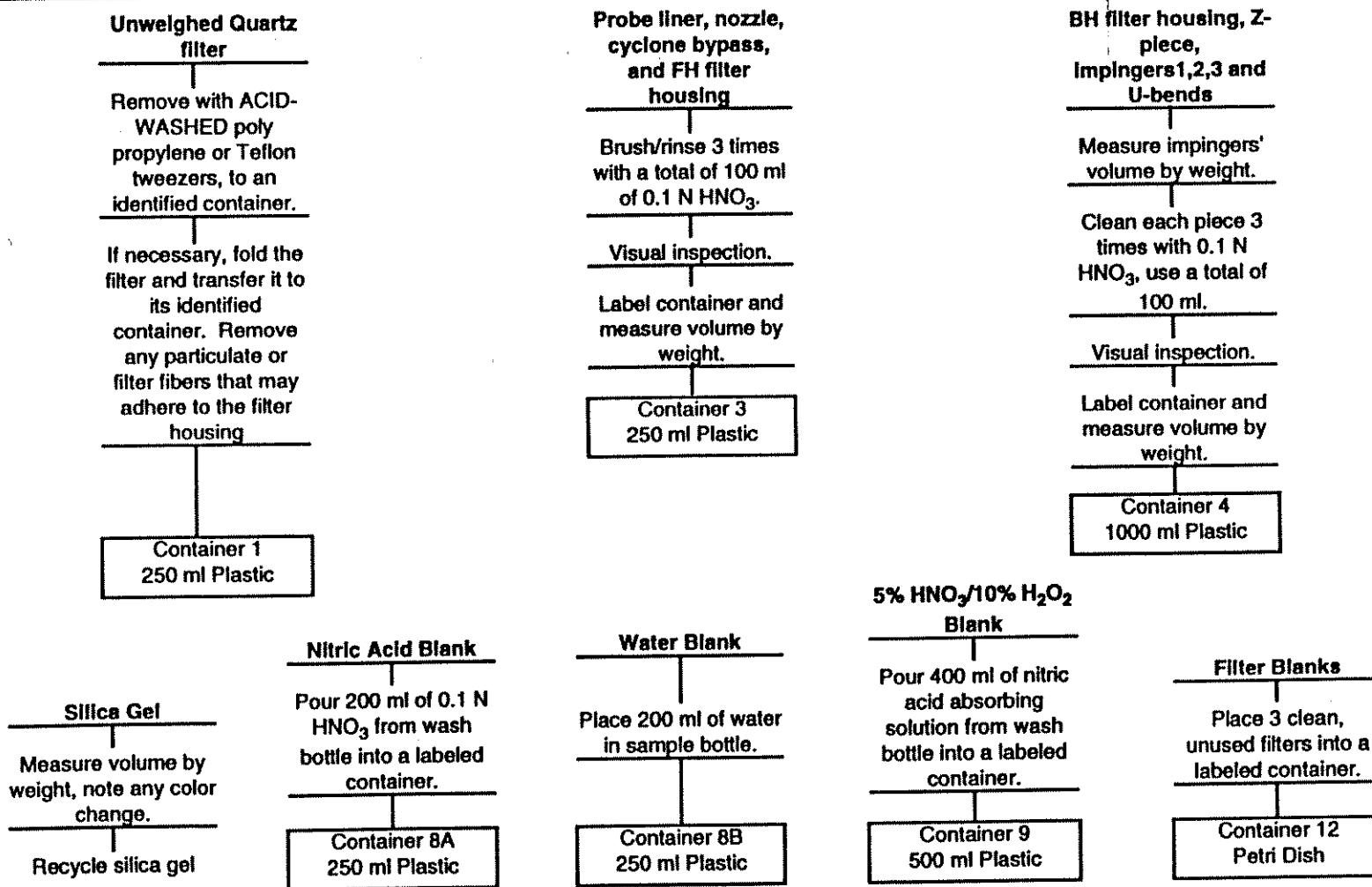
Impinger 1
Impinger 2
Impinger 3
Impinger 4
Impinger 5

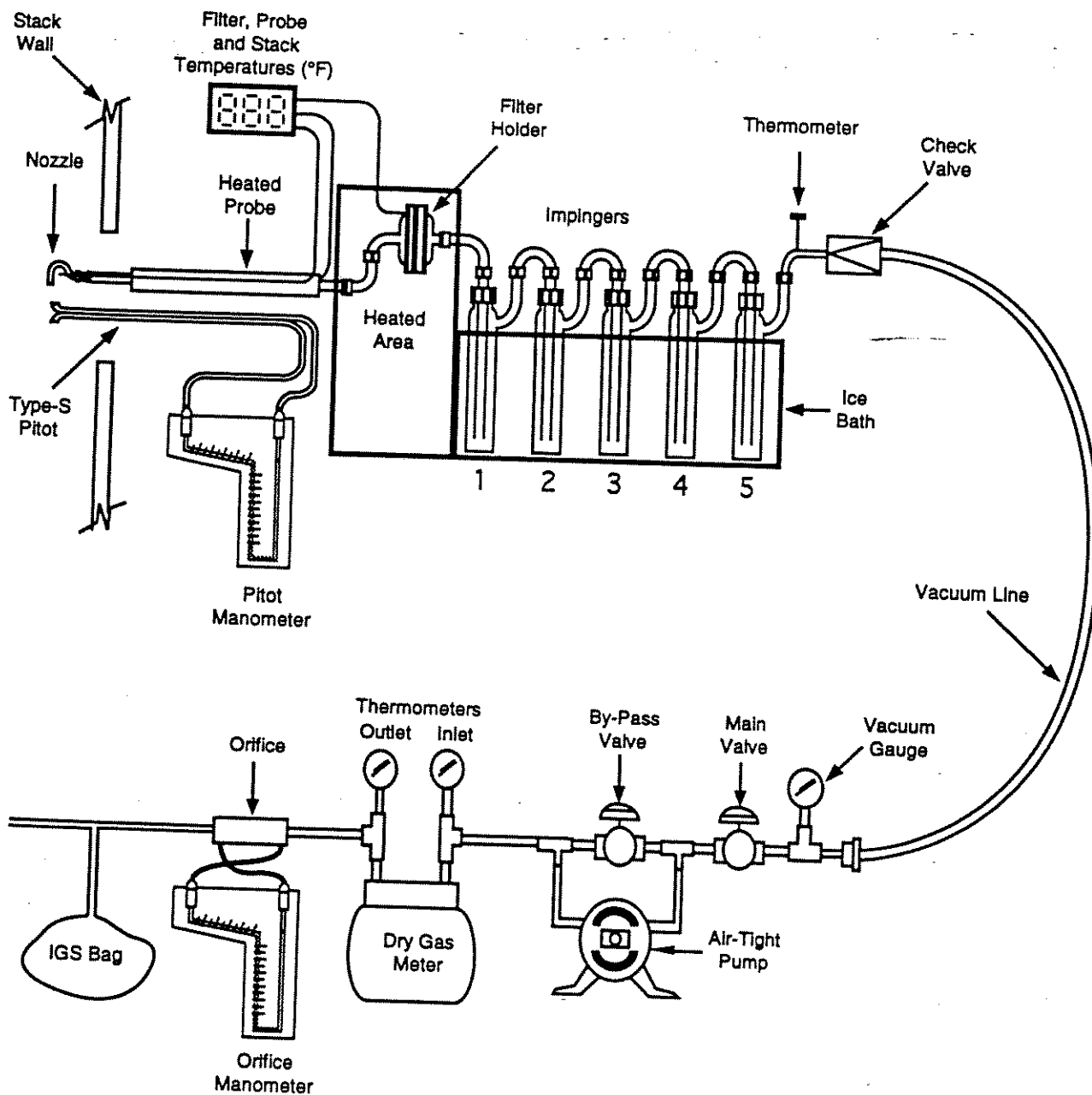
empty
100 ml 5% HNO_3 /10% H_2O_2
100 ml 5% HNO_3 /10% H_2O_2
empty
silica gel

METHOD 29 - DETERMINATION OF METALS EMISSIONS FROM STATIONARY SOURCES

(EXCLUDING MERCURY DETERMINATION, EXCLUDING PARTICULATE DETERMINATION)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





Proposed EPA Method 29 - Metals

Metals absorbing soln (5% HNO_3 /10% H_2O_2)

Mix 50 ml concentrated nitric acid (HNO_3) in 500 ml of DIUF water, add 333 ml of 30% H_2O_2 and dilute to 1 liter

Impinger 1
Impinger 2
Impinger 3
Impinger 4
Impinger 5

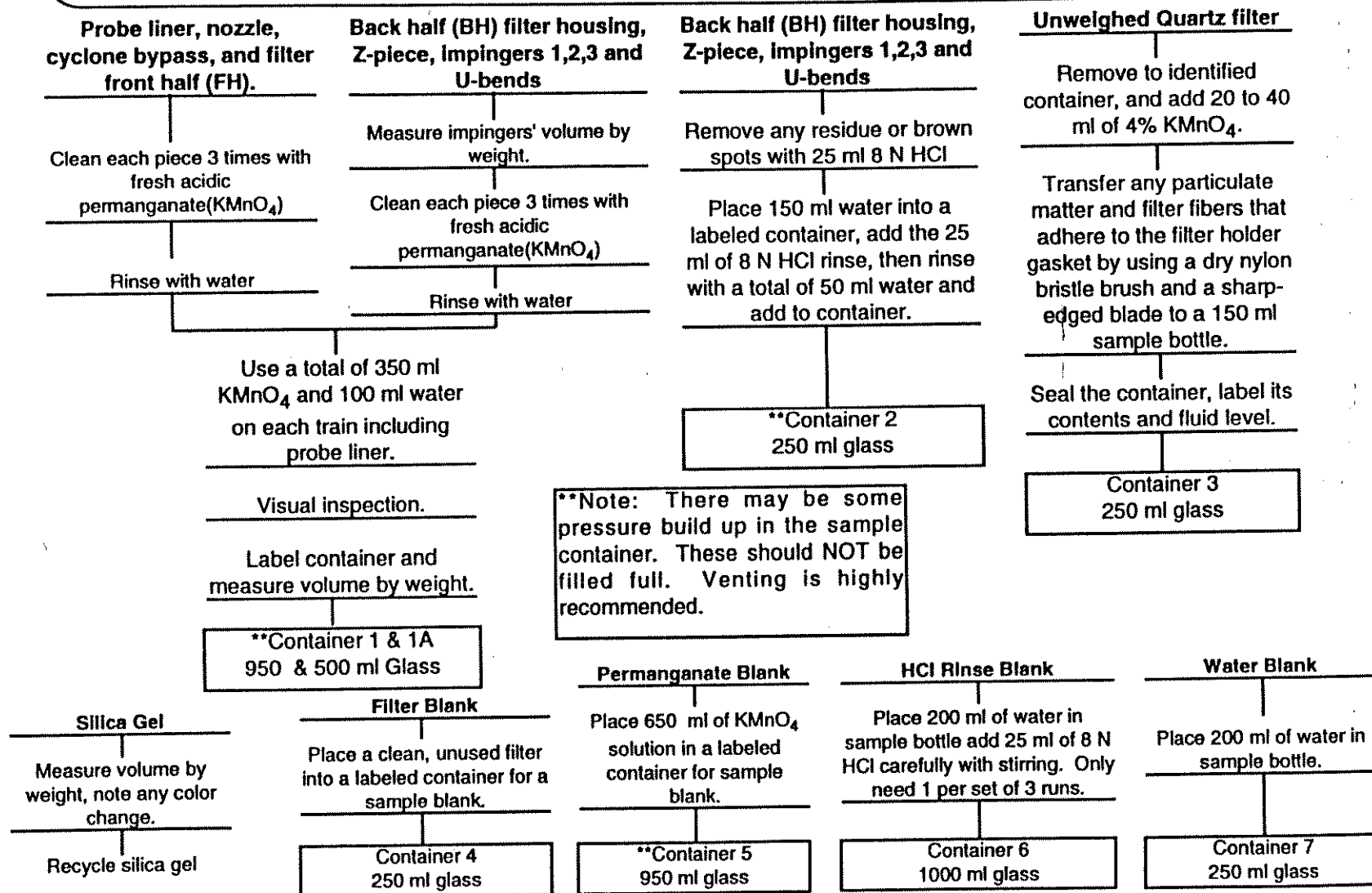
empty
100 ml 5% HNO_3 /10% H_2O_2
100 ml 5% HNO_3 /10% H_2O_2
empty
silica gel

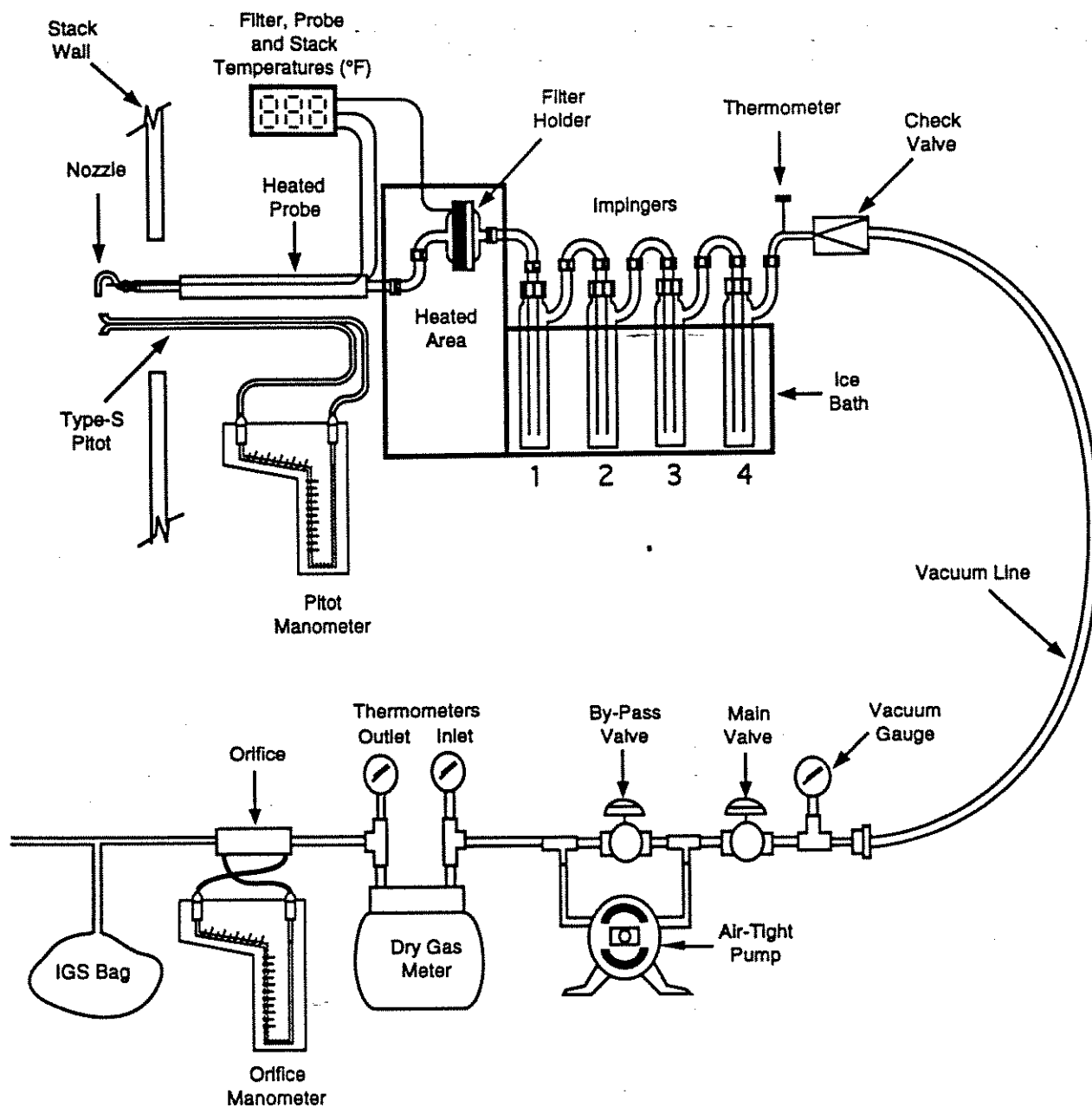
METHOD TOTAL: DETERMINATION OF PARTICULATE AND GASEOUS MERCURY EMISSIONS FROM SEWAGE SLOUGH

INCINERATORS.

(For M101A Train with Filter)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M101A- Mercury
absorbing solution (4% KMnO_4 /10% H_2SO_4)

Dissolve, with stirring, 40 grams potassium permanganate (KMnO_4) in 900 ml of DIUF water. Slowly add 100 ml concentrated sulfuric acid (H_2SO_4) and mix well, just prior to testing.

rinse solution (8N HCl)

Add 69 ml of concentrated HCl to 25 ml of DIUF water (Add acid to water). Dilute with water to 100 ml.

Impinger 1
Impinger 2
Impinger 3
Impinger 4

50 ml 4% KMnO_4 /10% H_2SO_4
100 ml 4% KMnO_4 /10% H_2SO_4
100 ml 4% KMnO_4 /10% H_2SO_4
silica gel

METHOD 101A -

**DETERMINATION OF PARTICULATE AND GASEOUS MERCURY
EMISSIONS FROM SEWAGE SLUDGE INCINERATORS
(FOR M101A TRAIN WITHOUT A FILTER)**

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

**Probe liner, nozzle,
cyclone bypass, and filter
bypass**

Clean each piece 3 times
with fresh acidic
permanganate(KMnO_4)

Rinse with water

**Filter bypass, Z-piece,
Impingers 1,2,3 and U-bends**

Measure impingers' volume by
weight.

Clean each piece 3 times with
fresh acidic
permanganate(KMnO_4)

Rinse with water

**Filter bypass, Z-piece,
Impingers 1,2,3 and U-bends**

Remove any residue or brown
spots with 25 ml 8 N HCl

Place 150 ml water into a
labeled container, add the 25
ml of 8 N HCl rinse, then rinse
with a total of 50 ml water and
add to container.

****Container 2
250 ml glass**

Use a total of 350 ml
 KMnO_4 and 100 ml water
on each train including
probe liner.

Visual inspection.

Label container and
measure volume by weight.

****Container 1 & 1A
950 ml Glass (2)**

****Note:** There may be some
pressure build up in the sample
container. These should NOT be
filled full. Venting is highly
recommended.

Permanganate Blank

Place 650 ml of KMnO_4
solution in a labeled
container for sample
blank.

****Container 5
950 ml Glass**

HCl Rinse Blank

Place 200 ml of water in
sample bottle add 25 ml of
8 N HCl carefully with
stirring. Need only 1 for 3
runs.

**Container 6
1000 ml glass**

Water Blank

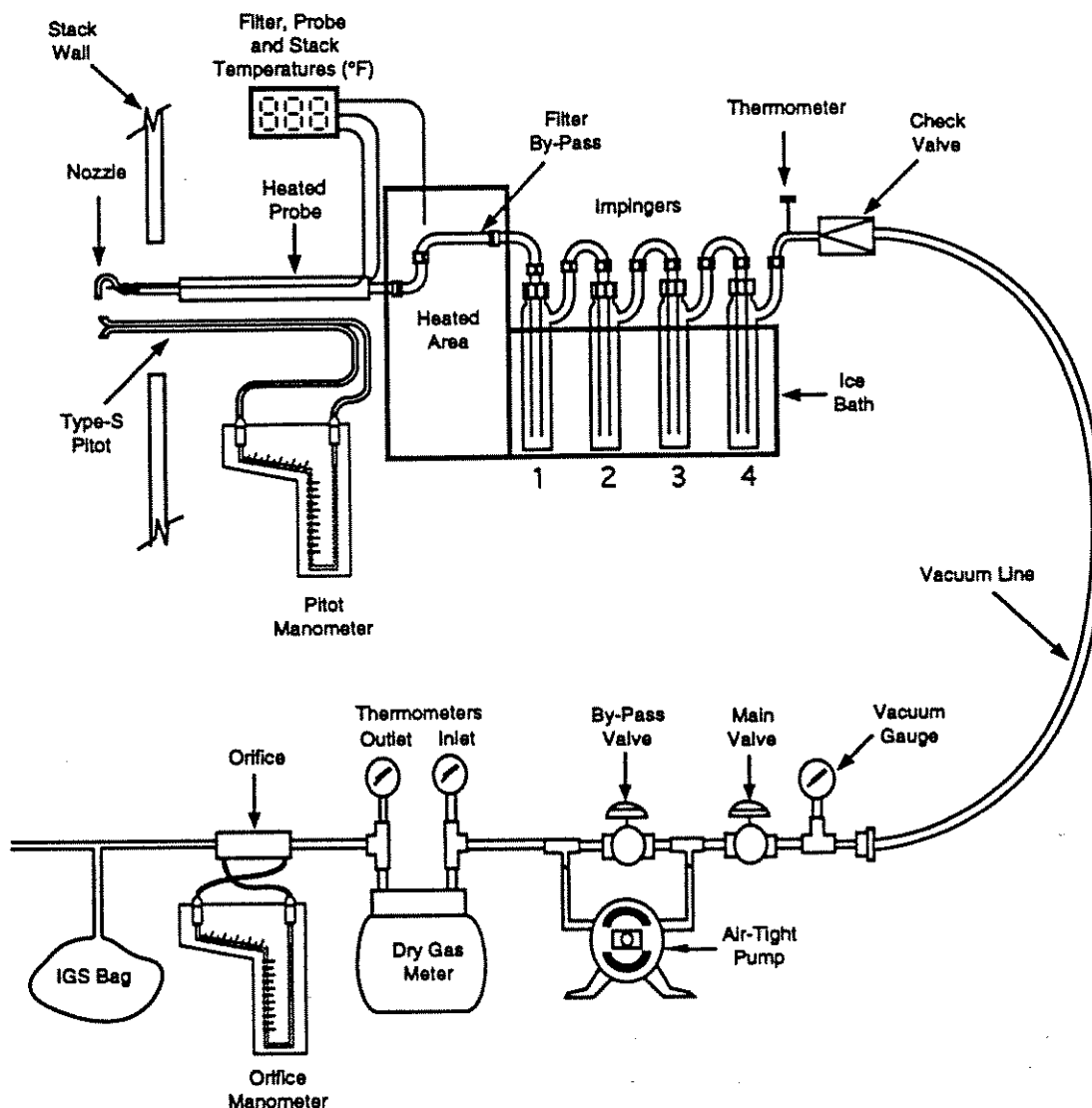
Place 200 ml of water in
sample bottle.

**Container 7
250 ml glass**

Silica Gel

Measure volume by
weight, note any color
change.

Recycle silica gel



M101A- Mercury
absorbing solution (4% KMnO_4 /10% H_2SO_4)

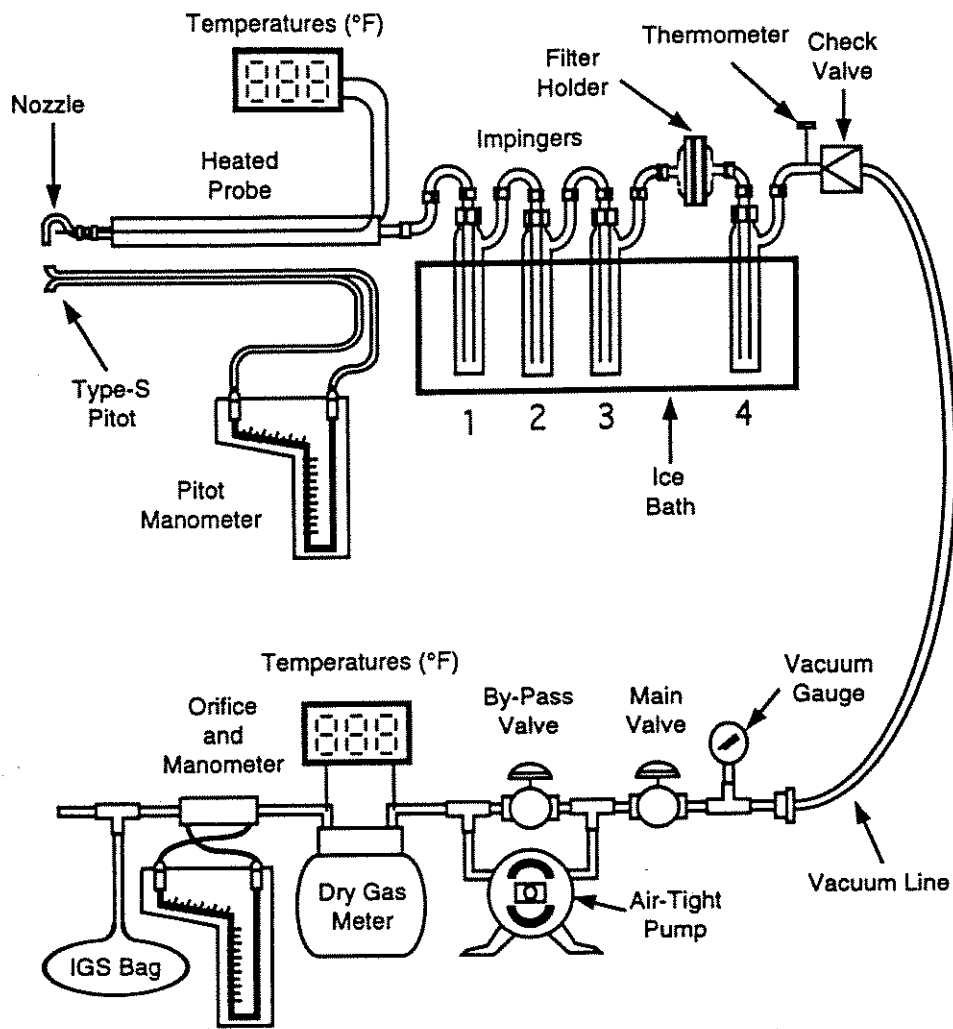
Dissolve, with stirring, 40 grams potassium permanganate (KMnO_4) in 900 ml of DIUF water. Slowly add 100 ml concentrated sulfuric acid (H_2SO_4) and mix well, just prior to testing.

rinse solution (8N HCl)

Add 69 ml of concentrated HCl to 25 ml of DIUF water (Add acid to water). Dilute with water to 100 ml.

Impinger 1
Impinger 2
Impinger 3
Impinger 4

50 ml 4% KMnO_4 /10% H_2SO_4
100 ml 4% KMnO_4 /10% H_2SO_4
100 ml 4% KMnO_4 /10% H_2SO_4
silica gel



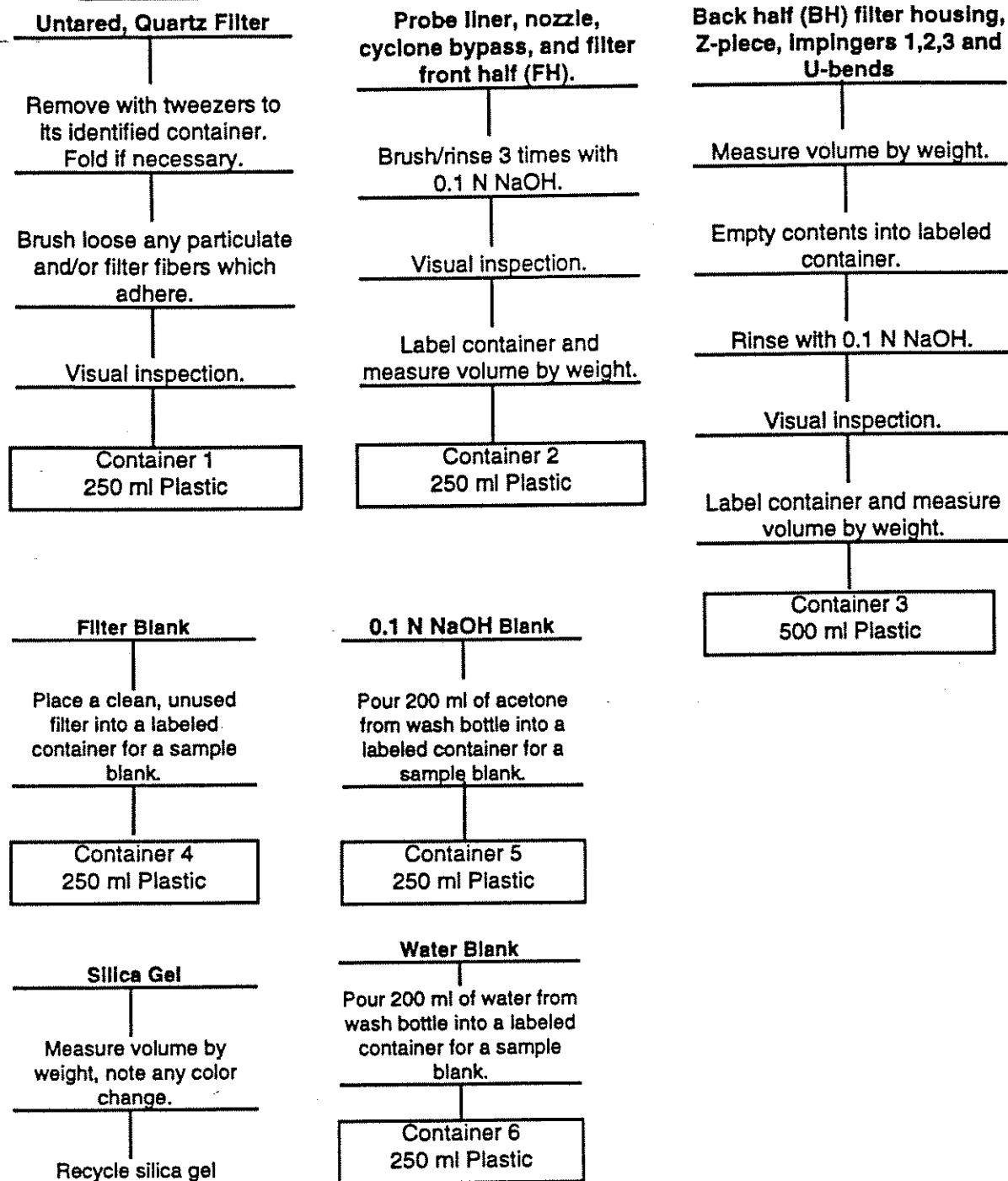
M104 - Beryllium (Be)

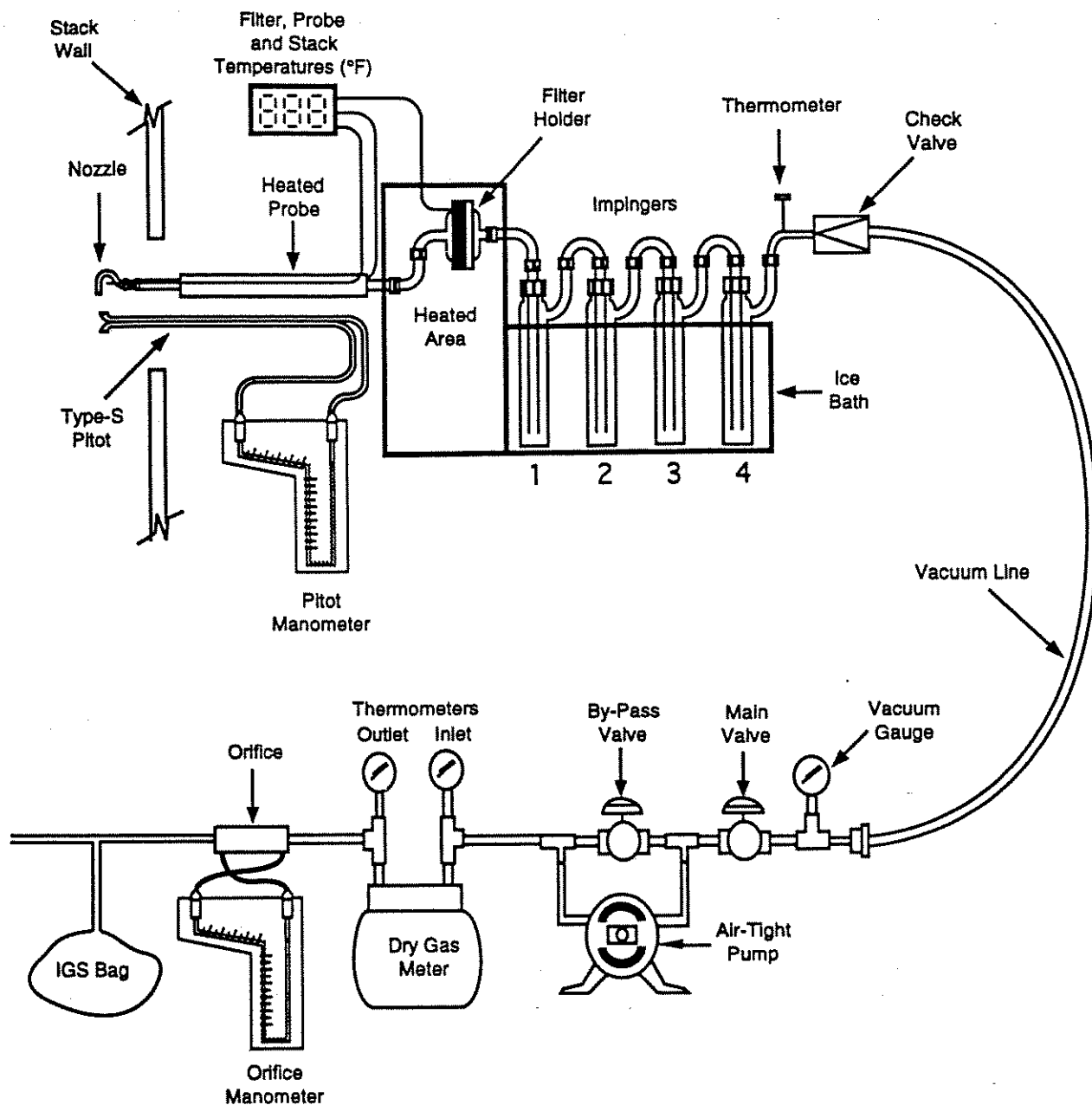
Impinger 1
Impinger 2
Impinger 3
Impinger 4

100 ml H₂O
100 ml H₂O
empty
silica gel

METHOD 108 - Determination of Particulate and Gaseous Arsenic Emissions

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M108 - Arsenic (As)

Impinger 1
Impinger 2
Impinger 3
Impinger 4

100 ml H₂O
100 ml H₂O
empty
silica gel

METHOD 201A - DETERMINATION OF PM₁₀ EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Tared, Glass Fiber Filter

Remove with tweezers to its identified container.
Fold if necessary.

Brush loose any particulate and/or filter fibers which adhere.

Visual inspection.

Container 1
Petri Dish

(PM₁₀ Rinse) filter FH, turnaround cup FH, exit of cyclone

Brush/rinse 3 times with acetone.

Visual inspection.

Label container and measure volume by weight.

Container 2
125 ml Glass

(Total Rinse) cyclone, nozzle

Brush/rinse 3 times with acetone.

Visual inspection.

Label container and measure volume by weight.

Container 3
125 or 60 ml Glass

Filter BH, Z-piece, Impingers 1, 2, 3 and U-bends

Measure volume by weight.

Empty contents into labeled container.

Rinse with water.

Visual inspection.

Label container and measure volume by weight.

Container 4*
500 ml Glass

*Container 4 only if recovering back-half

Filter Blank

Place a clean, unused tared filter into a labeled container for a sample blank.

Container 5
Petri Dish

Acetone Blank

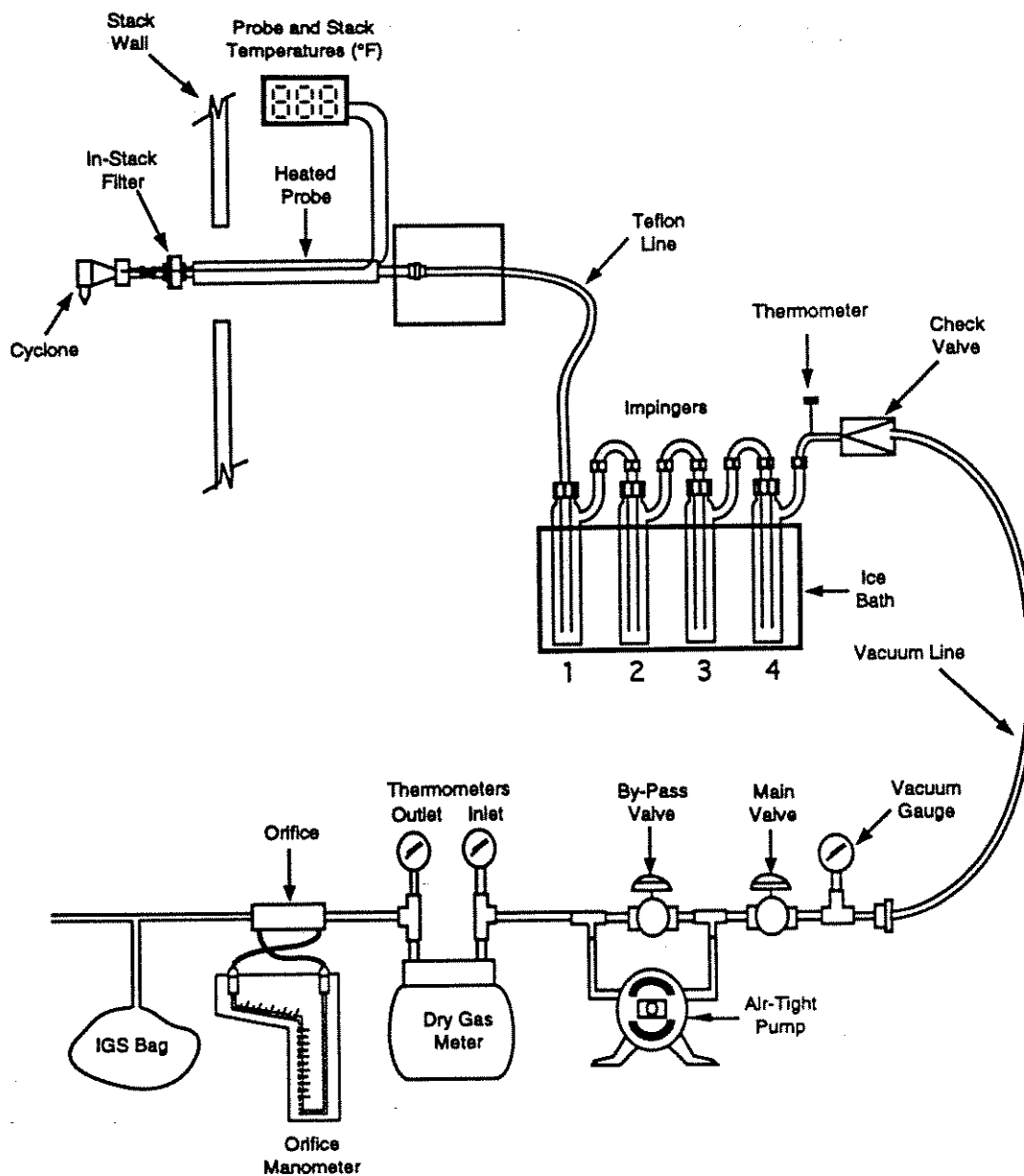
Pour 200 ml of acetone from wash bottle into a labeled container for a sample blank.

Container 6
250 ml Glass

Silica Gel

Measure volume by weight, note any color change.

Recycle silica gel



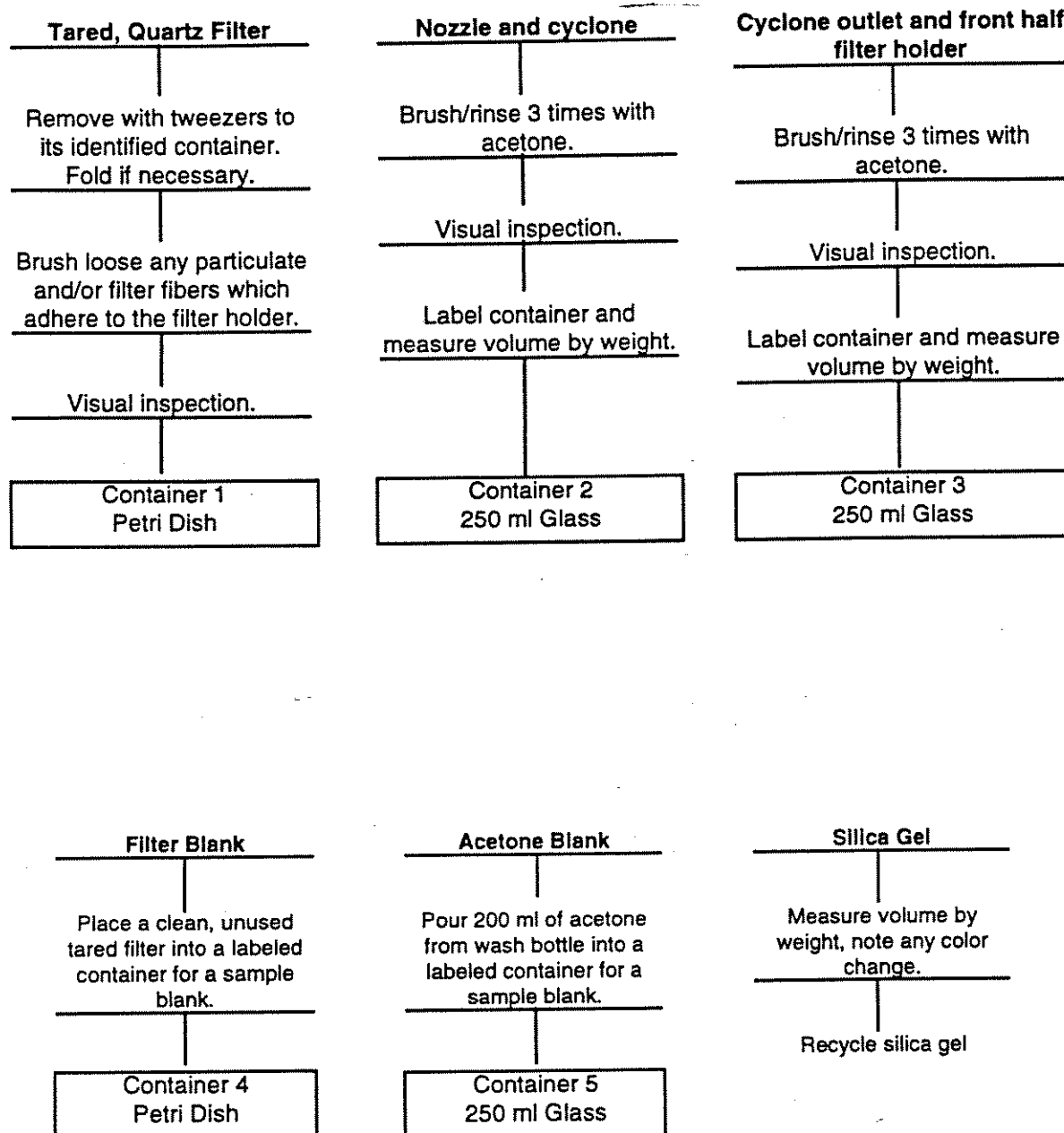
M201A - PM₁₀

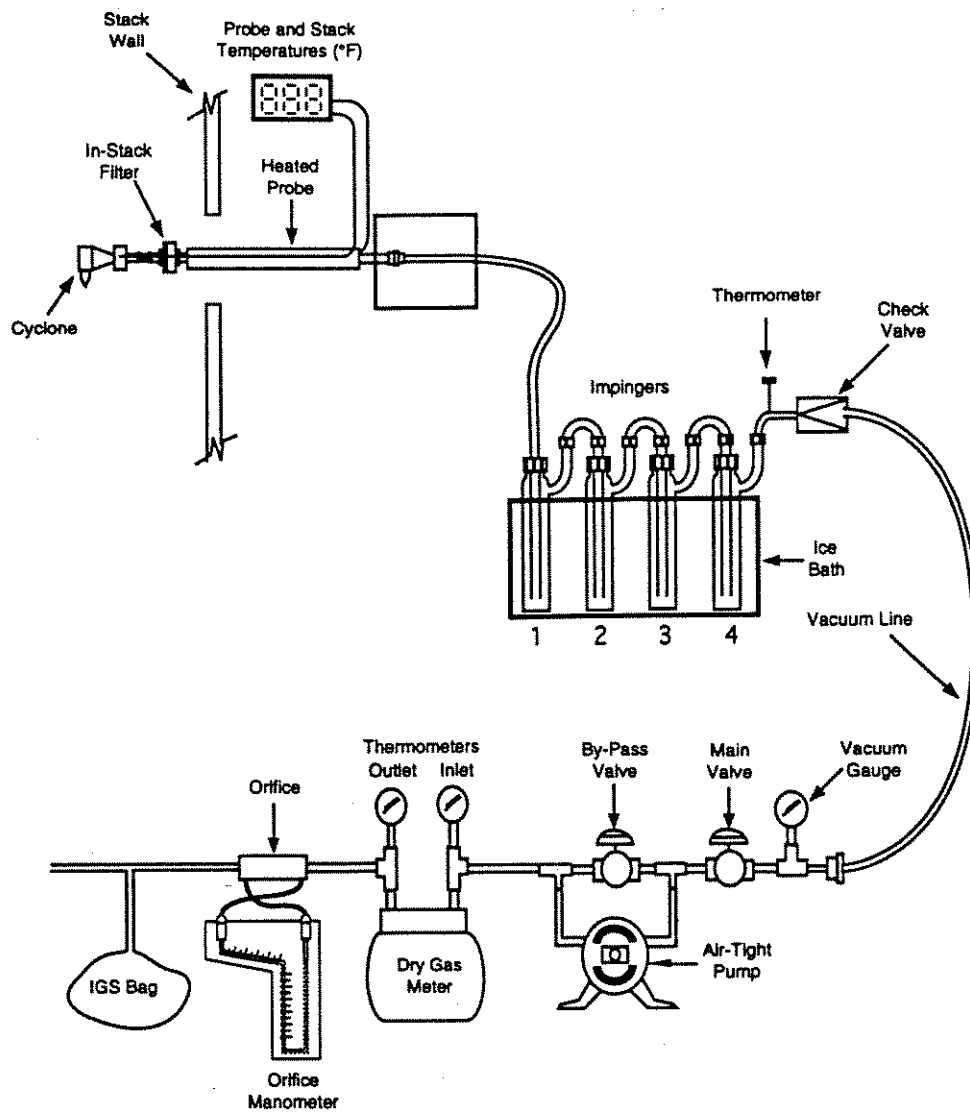
Impinger 1
 Impinger 2
 Impinger 3
 Impinger 4

100 ml H₂O
 100 ml H₂O
 empty
 silica gel

METHOD 201A - DETERMINATION OF PM₁₀ EMISSIONS FROM STATIONARY SOURCES
(NOT INCLUDING BACK HALF)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).



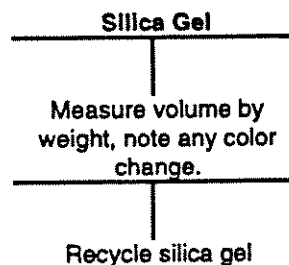
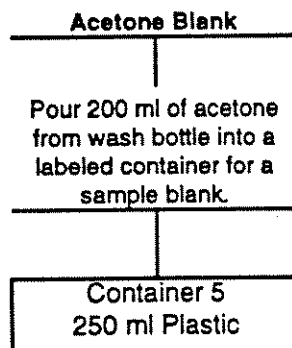
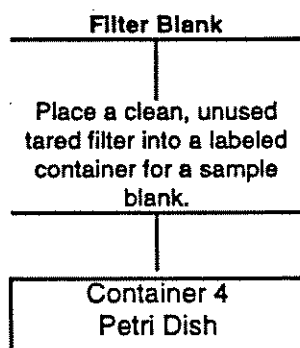
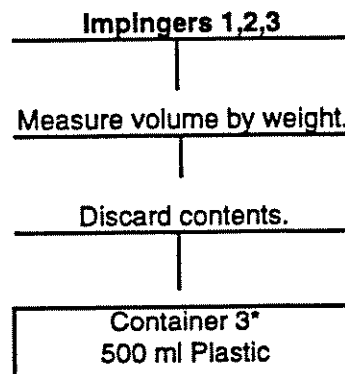
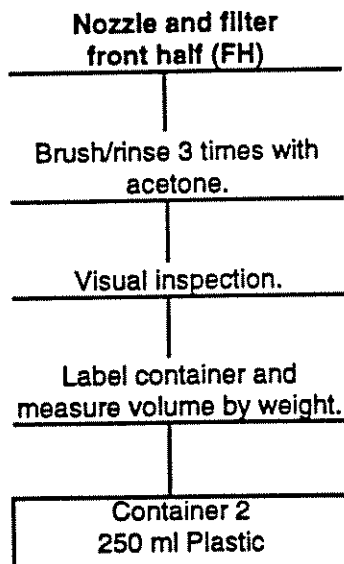
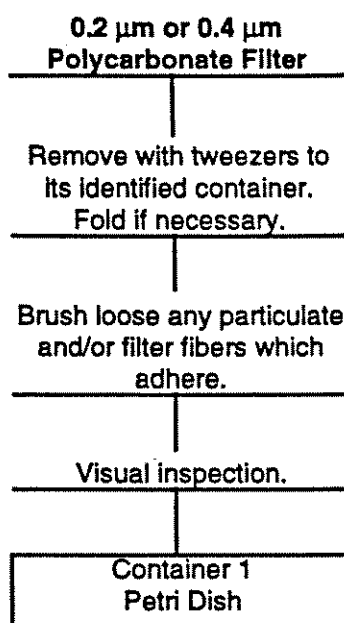


M201A - PM₁₀

Impinger 1	100 ml H ₂ O
Impinger 2	100 ml H ₂ O
Impinger 3	empty
Impinger 4	silica gel

METHOD 427 - DETERMINATION OF ASBESTOS EMISSIONS FROM STATIONARY SOURCES

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).



- 1 pair of each set of blanks per 6 pairs of tested traps.
- Mark direction of flow on Tenax cartridges with a PENCIL.

**Tenax and
Tenax/Charcoal sorbent
cartridges**

Remove both sorbent
cartridges. Replace end
caps and label accordingly.

Keep cartridges on cold
packs until they are ready
for analysis.

Containers 1 & 2

Field Blanks

Blank Tenax and
Tenax/charcoal traps are
taken to sampling site; end
caps are removed for the
period of time required to
exchange two pairs of traps
on VOST.

After the exchange, replace
the end caps and label
accordingly.

Keep cartridges on cold
packs until they are ready
for analysis.

Containers 3 & 4

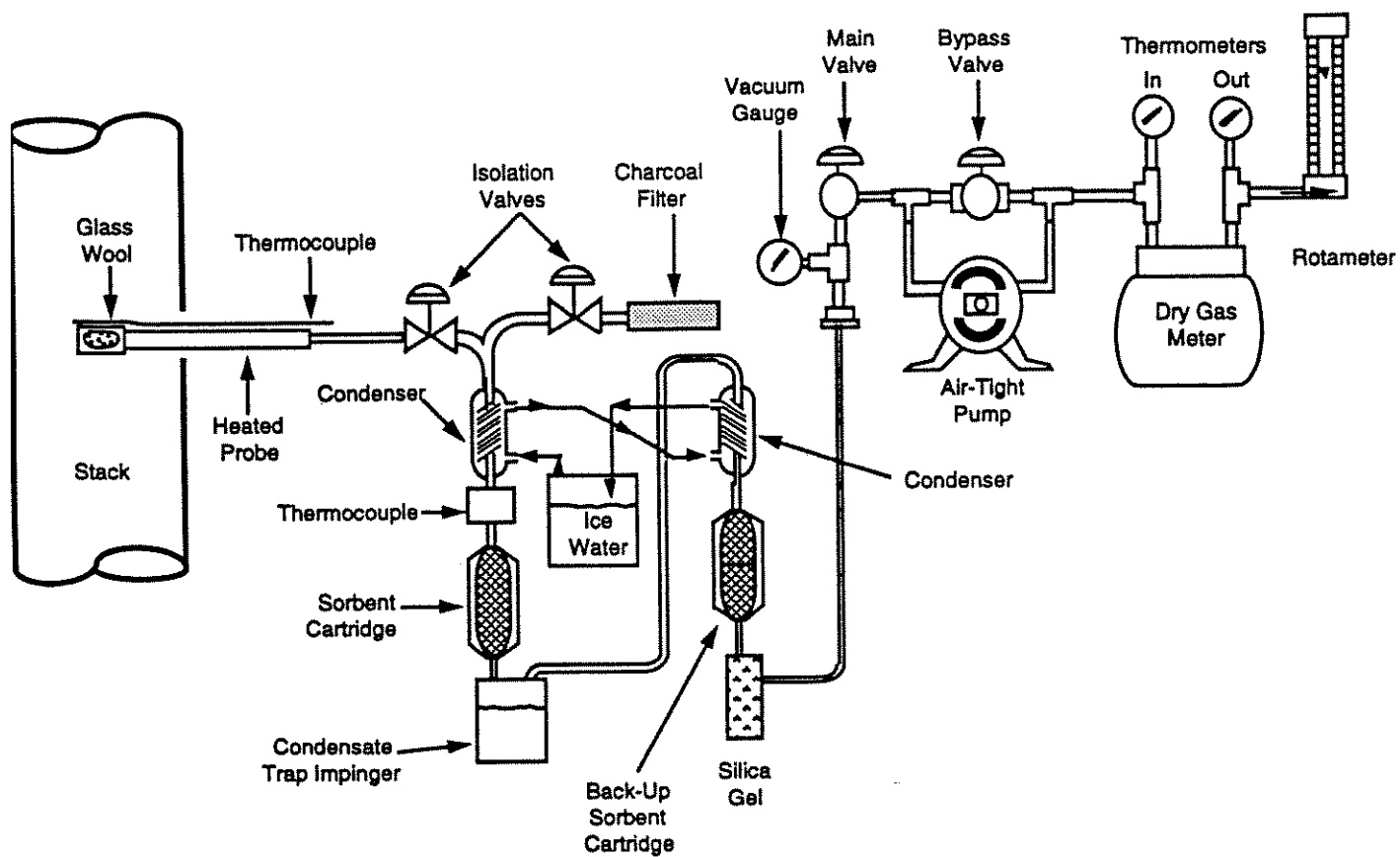
Trip Blanks

At least one pair of blank
cartridges shall be included
with shipment of cartridges
to the site. The end caps
will NOT be removed.

Keep cartridges on cold
packs until they are ready
for analysis.

Containers 5 & 6

Note: If condensate is collected, place it in a 20 or 40 ml VOA vial. Fill the vial to the top with HPLC water so that no air is present in the vial.



METHOD 0050 - ISOKINETIC HCl/Cl₂ EMISSION SAMPLING TRAIN
(INCLUDING PARTICULATE EMISSIONS, EXCLUDING Cl₂ EMISSIONS)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Weighed Quartz Filter

Remove with tweezers to its identified container.
Fold if necessary.

Brush loose any particulate and/or filter fibers which adhere.

Visual inspection.

Container 1
Petri Dish

Probe liner, nozzle, cyclone bypass, and filter front half (FH).

Brush/rinse 3 times with acetone.

Visual inspection.

Label container and measure volume by weight.

Container 2
250 ml Glass

Back half (BH) filter housing, Z-piece, impingers 1,2,3 and U-bends

Measure volume by weight.

Empty contents into glass container.

Rinse with water.

Visual inspection.

Label container and measure volume by weight.

Container 3
500 ml Glass

Filter Blank

Place a clean, unused filter into a labeled container for a sample blank.

Container 4
Petri Dish

0.1 N H₂SO₄ Blank

Pour 200 ml of 0.1N H₂SO₄ into a labeled container for a sample blank.

Container 5
250 ml glass

Water Blank

Pour 200 ml of water from wash bottle into a labeled container for a sample blank.

Container 6
250 ml Glass

Acetone Blank

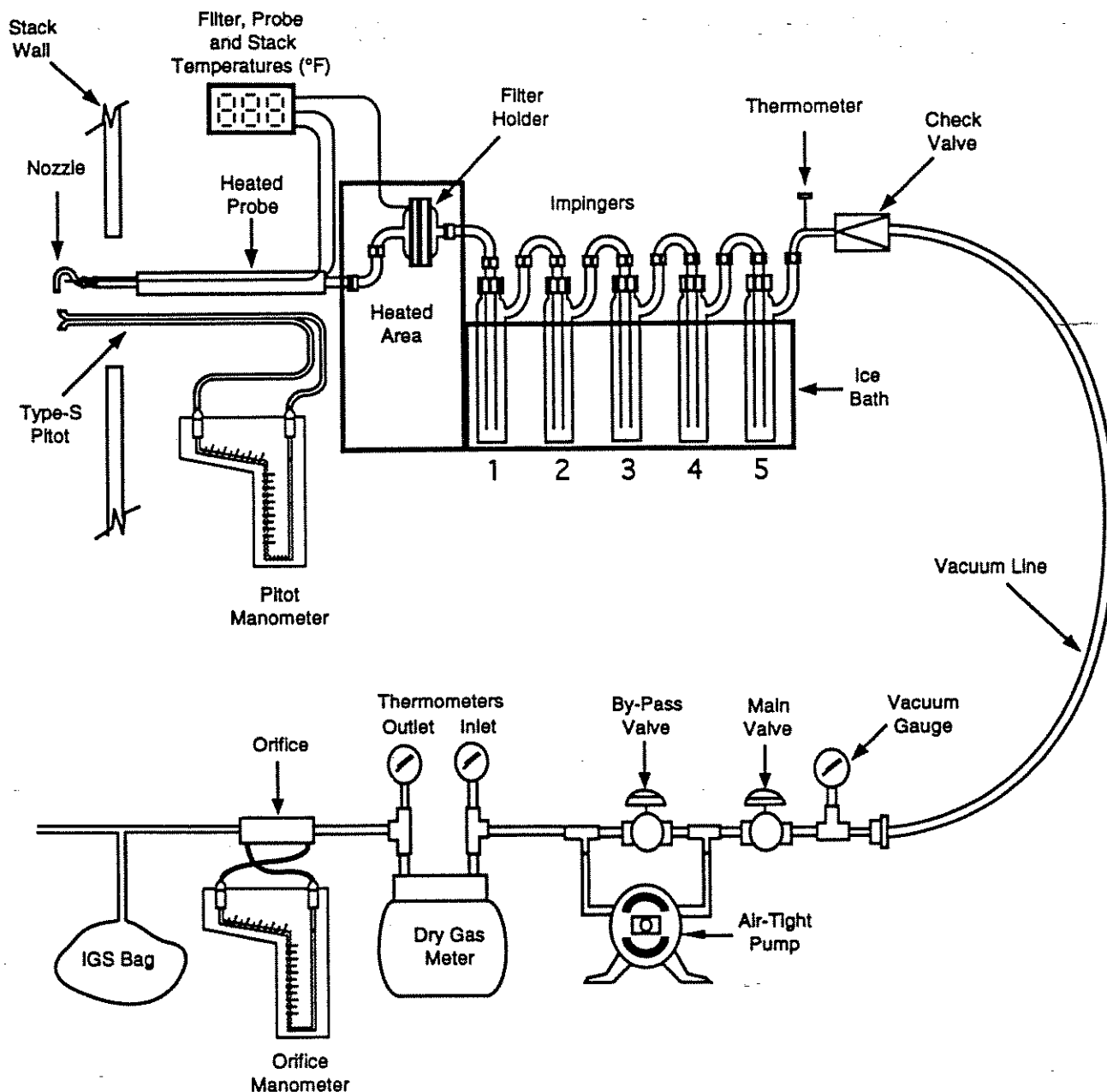
Pour 200 ml of acetone from wash bottle into a labeled container for a sample blank.

Container 7
250 ml Glass

Silica Gel

Measure volume by weight, note any color change.

Recycle silica gel



M0050 - Particulate/Hydrogen Chloride/Chlorine

HCl absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

Cl_2 absorbing solution (0.1 N NaOH)

Dissolve 4.0 grams of solid NaOH in approximately 1000 ml of DI water. Shake well to mix the solution.

Impinger 1

Impinger 2 (1)

Impinger 3 (2)

Impinger 4 (3)

Impinger 5 (4)

Impinger 6 (5)

50 ml 0.1 N H_2SO_4 (OPTIONAL)

100 ml 0.1 N H_2SO_4

100 ml 0.1 N H_2SO_4

100 ml 0.1 N NaOH

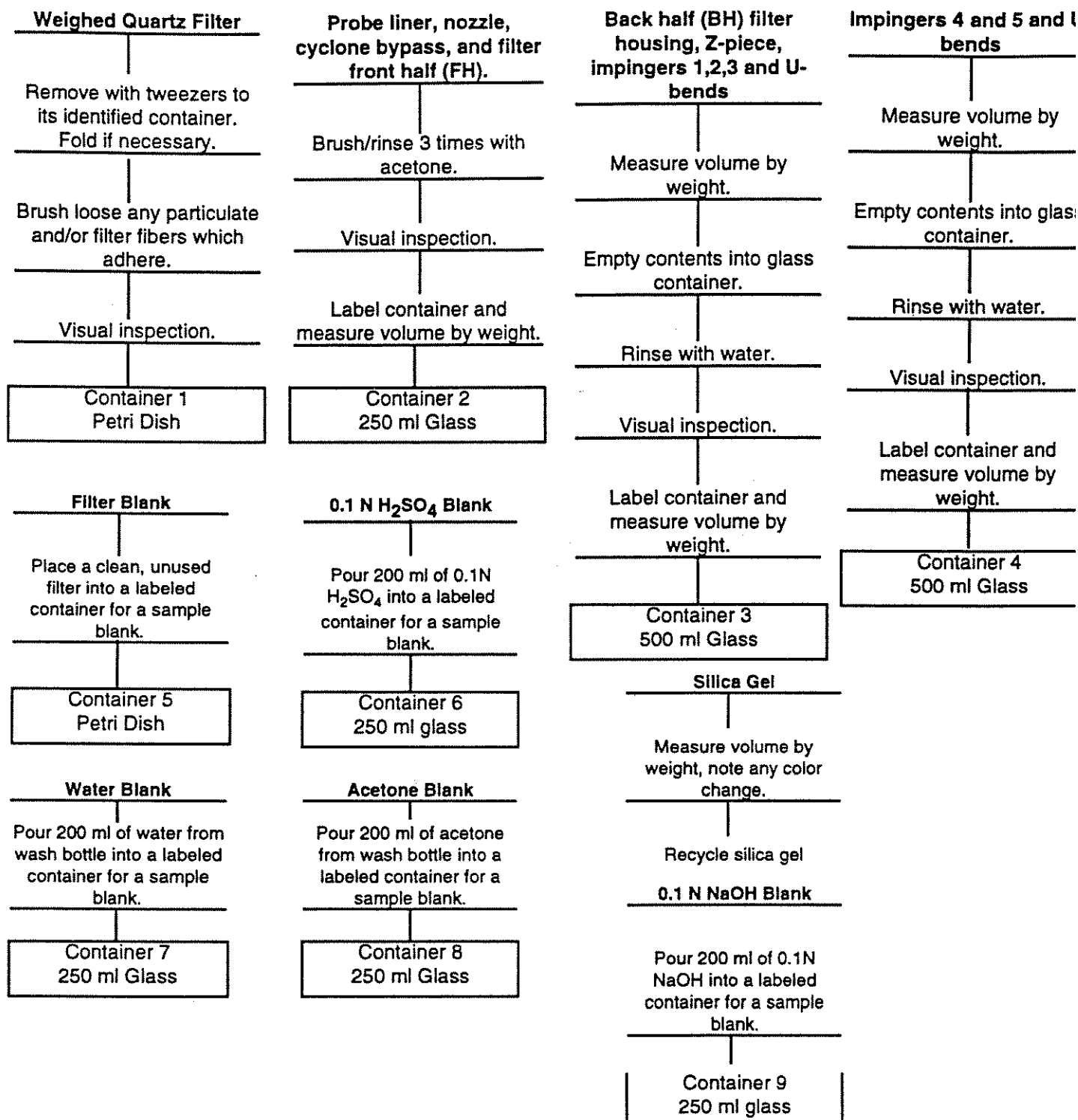
100 ml 0.1 N NaOH

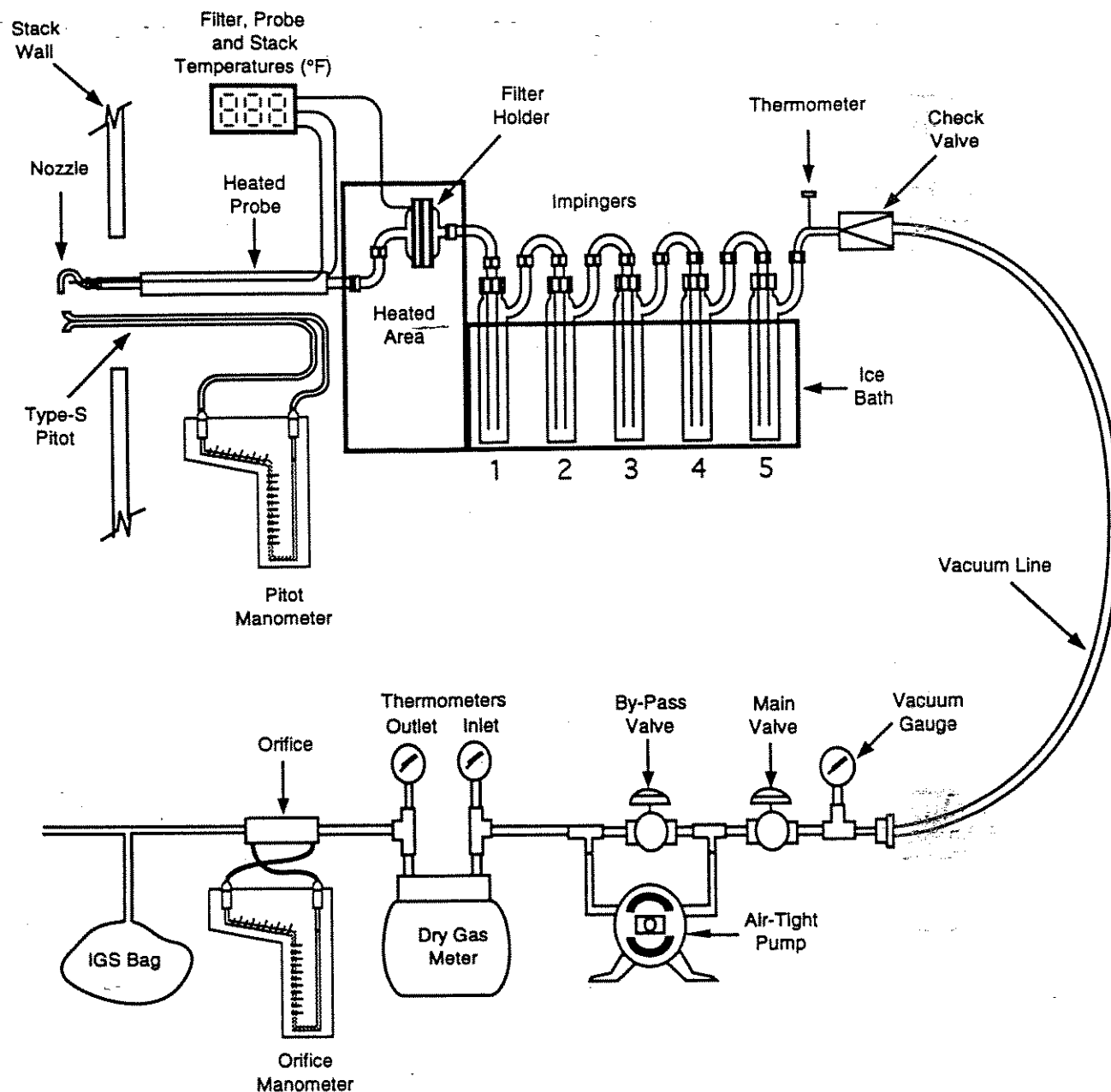
silica gel

Note: This is a traversing, isokinetic sampling train.

METHOD 0050 - ISOKINETIC HCl/Cl₂ EMISSION SAMPLING TRAIN
(INCLUDING PARTICULATE EMISSIONS, INCLUDING Cl₂ EMISSIONS)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).





M0050 - Particulate/Hydrogen Chloride/Chlorine

HCl absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

Cl_2 absorbing solution (0.1 N NaOH)

Dissolve 4.0 grams of solid NaOH in approximately 1000 ml of DI water. Shake well to mix the solution.

Impinger 1

50 ml 0.1 N H_2SO_4 (OPTIONAL)

Impinger 2 (1)

100 ml 0.1 N H_2SO_4

Impinger 3 (2)

100 ml 0.1 N H_2SO_4

Impinger 4 (3)

100 ml 0.1 N NaOH

Impinger 5 (4)

100 ml 0.1 N NaOH

Impinger 6 (5)

silica gel

Note: This is a traversing, isokinetic sampling train.

METHOD 0051 - HCl/Cl₂ EMISSION SAMPLING TRAIN
(INCLUDING PARTICULATE EMISSIONS, EXCLUDING Cl₂ EMISSIONS)

- Tare all sample containers before sample collection.
- Mark all liquid levels and final weights on the outside of each sample container.
- Seal all sample containers with Teflon tape.
- If recycling, bake silica gel for two hours at 350° F (175° C).

Weighed Quartz Filter

Remove with tweezers to its identified container.
Fold if necessary.

Brush loose any particulate and/or filter fibers which adhere.

Visual inspection.

Container 1
Petri Dish

Probe liner, nozzle, cyclone bypass, and filter front half (FH).

Brush/rinse 3 times with acetone.

Visual inspection.

Label container and measure volume by weight.

Container 2
250 ml Glass

Back half (BH) filter housing, Z-piece, impingers 1,2,3 and U-bends

Measure volume by weight.

Empty contents into glass container.

Rinse with water.

Visual inspection.

Label container and measure volume by weight.

Container 3
500 ml Glass

Filter Blank

Place a clean, unused filter into a labeled container for a sample blank.

Container 4
Petri Dish

0.1 N H₂SO₄ Blank

Pour 200 ml of 0.1N H₂SO₄ into a labeled container for a sample blank.

Container 5
250 ml glass

Water Blank

Pour 200 ml of water from wash bottle into a labeled container for a sample blank.

Container 6
250 ml Glass

Acetone Blank

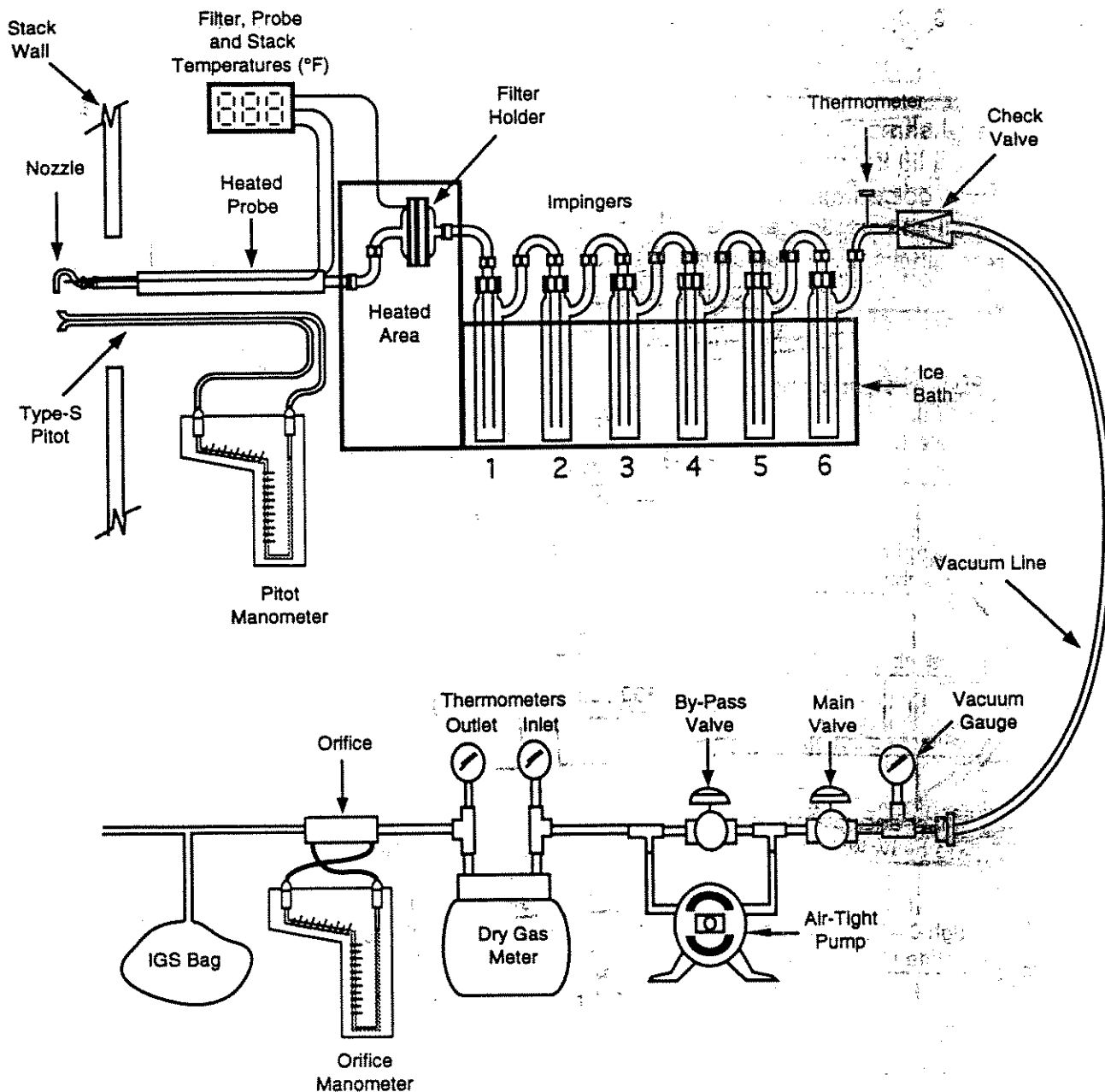
Pour 200 ml of acetone from wash bottle into a labeled container for a sample blank.

Container 7
250 ml Glass

Silica Gel

Measure volume by weight, note any color change.

Recycle silica gel



M0051 - Hydrogen Chloride/ Chlorine
HCl absorbing solution (0.1 N H_2SO_4)

Slowly add 2.8 ml concentrated sulfuric acid (H_2SO_4) to approximately 1000 ml DI water. Shake well to mix the solution.

Cl_2 Cl_2 absorbing solution (0.1 N NaOH)

Dissolve 4.0 grams of solid NaOH in approximately 1000 ml of DI water. Shake well to mix the solution.

Midget Impinger 1	empty
Midget Impinger 2	15 ml 0.1 N H_2SO_4
Midget Impinger 3	15 ml 0.1 N H_2SO_4
Midget Impinger 4	15 ml 0.1 N NaOH
Midget Impinger 5	15 ml 0.1 N NaOH
Midget Impinger 6	silica gel

Note: Because you are also sampling for particulate, this is an isokinetic sampling train.